

Roles of the Lenses

Gun Lens

Helps form probe

Condenser Lens

Mainly controls:
Spot Size
hence total beam
current

Objective Lens

Mainly control
probe focus

Diffraction/Intermediate Lens

Controls Mode

Projector Lens

Magnification



Most TEM/STEM
have 7-8 Lenses

2 Condensers
1 Objective
1-2 Intermediate
2 Projectors

Most instruments
have only
Electromagnetic
Round Lenses

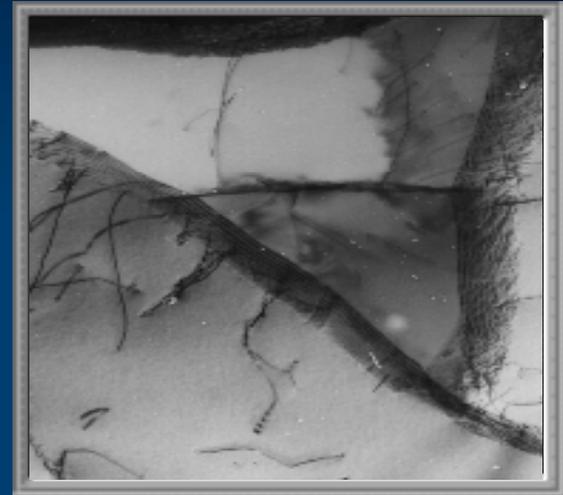
Note the locations
of the various
Apertures.

Optimum aperture
sizes are needed
for various
imaging functions.

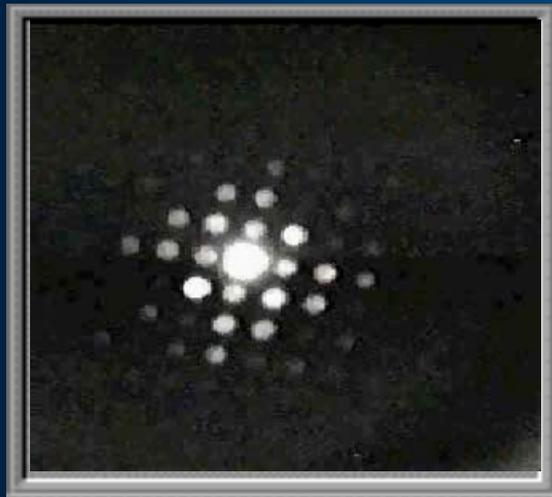
Transmission Electron Microscopy



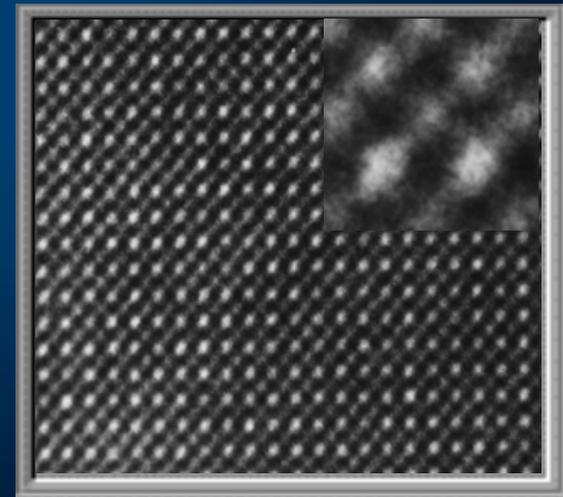
*Conventional
Imaging*



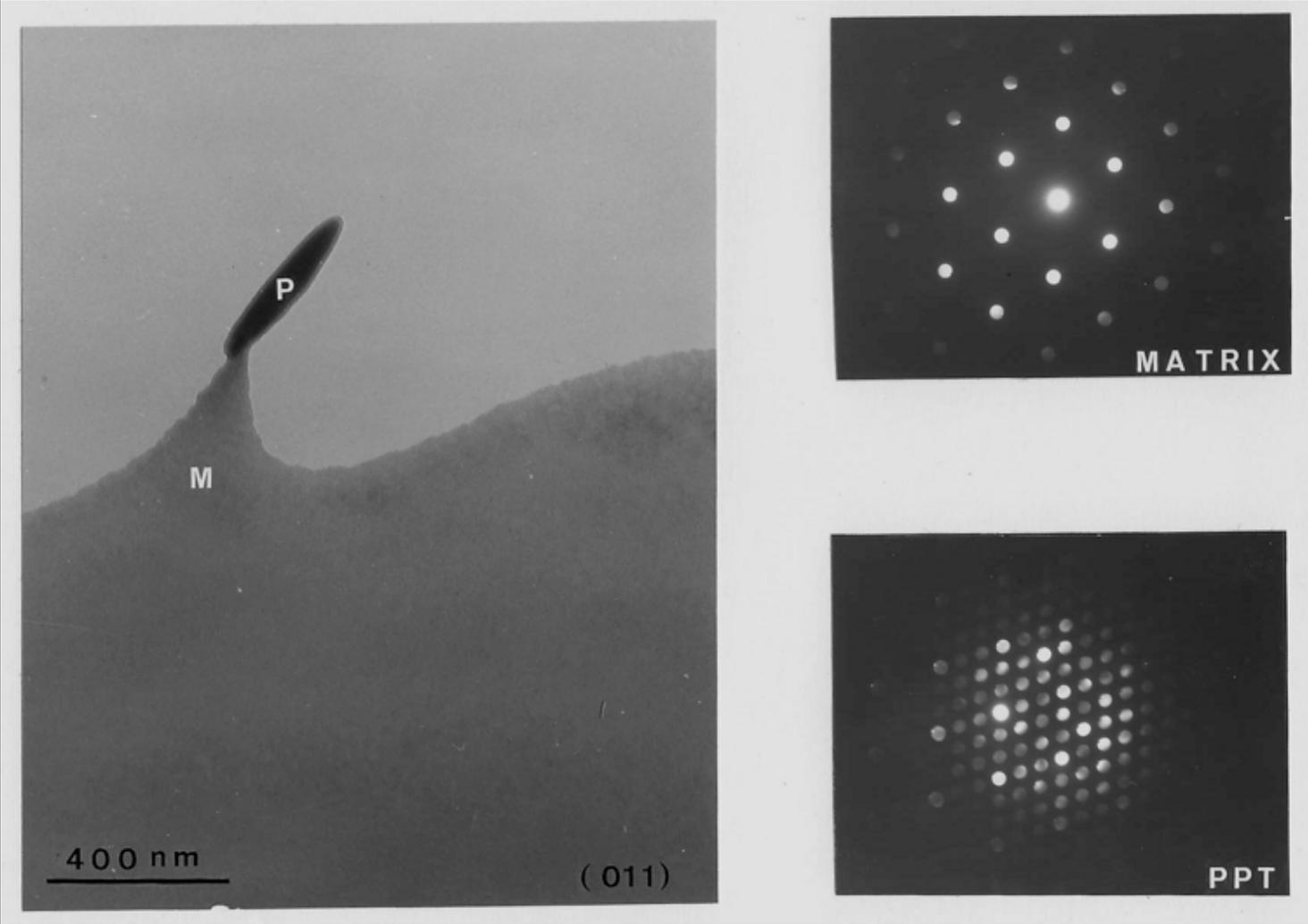
*High
Resolution
Imaging*



Diffraction

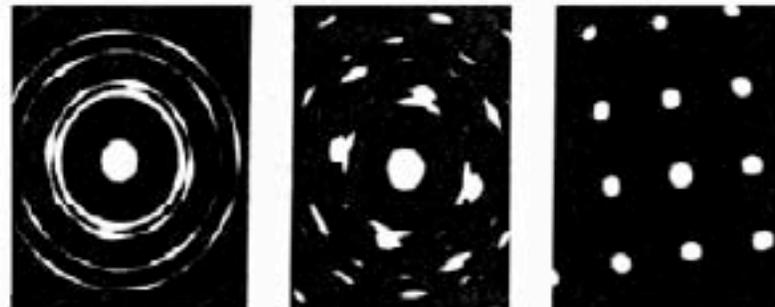
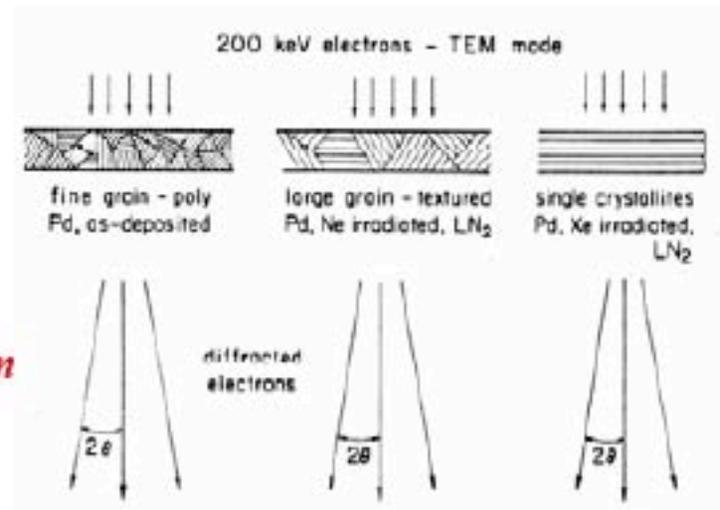


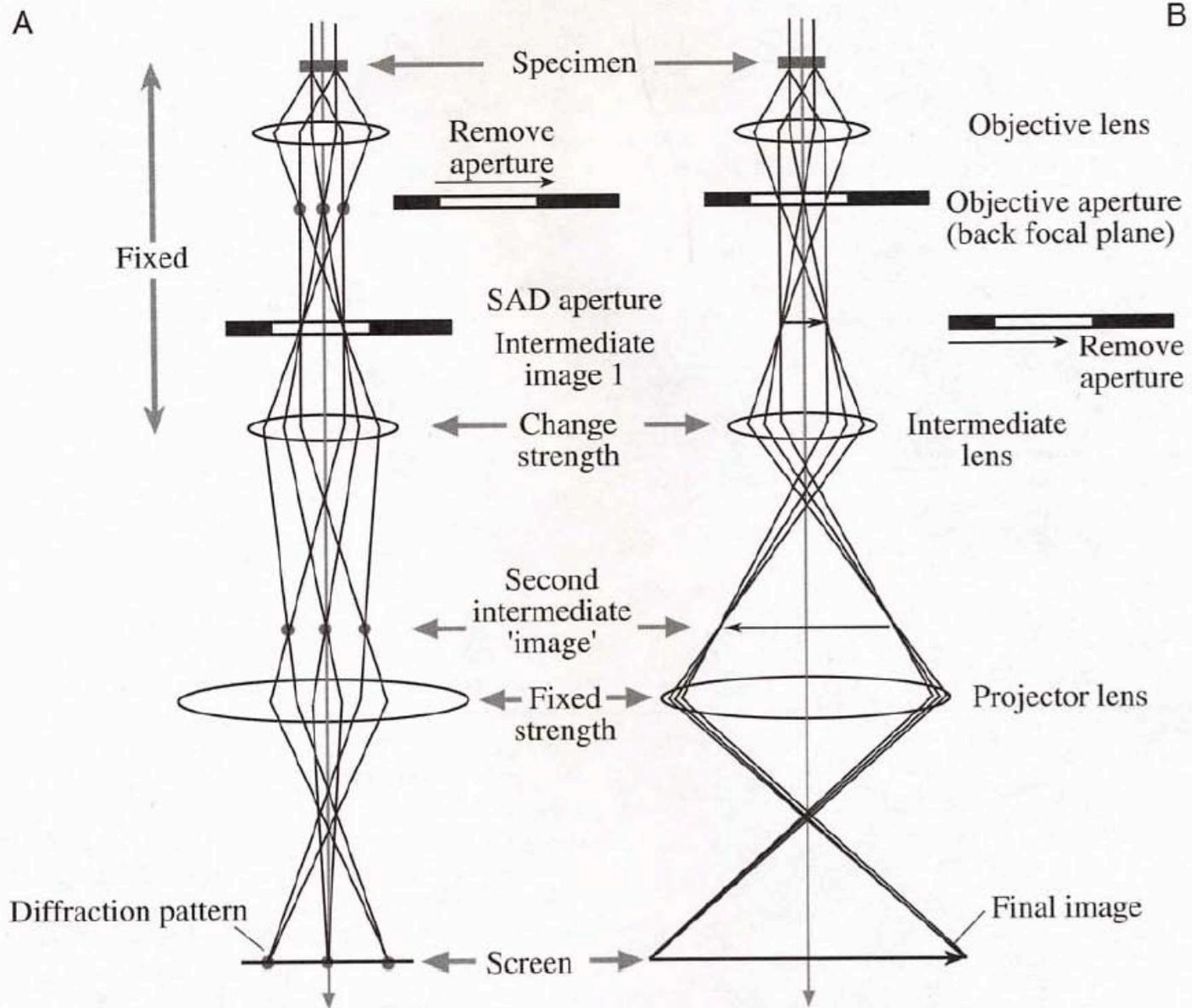
Electron Diffraction



1. Diffraction pattern capability is one of the most important features of the TEM, because we can relate the crystallography to the images obtained.
2. The ability to determine crystallographic orientations locally (down to the nm level) gives the TEM its great advantage over the SEM and visible-light microscopes.
3. The questions that we can address using diffraction patterns obtained in the TEM include the following:
 - Is the specimen crystalline? Crystalline and amorphous materials have very different properties.
 - If it is crystalline, then what are the crystallographic characteristics (lattice parameter, symmetry, etc.) of the specimen?
 - Is the specimen monocrystalline? If not, what is the grain morphology, how large are the grains, what is the grain-size distribution, etc?
 - What is the orientation of the specimen or of individual grains with respect to the electron beam?
 - Is more than one phase present in the specimen?

*Electron Beam
Diffraction of a Pd film*





Type of Electron Scattering	Angular Range	Energy Loss
Unscattered	0	0
Elastic	10's-100's mR	~0
Phonon	10's-100's mR	<.025 eV
Inelastic	10's mR	everything else

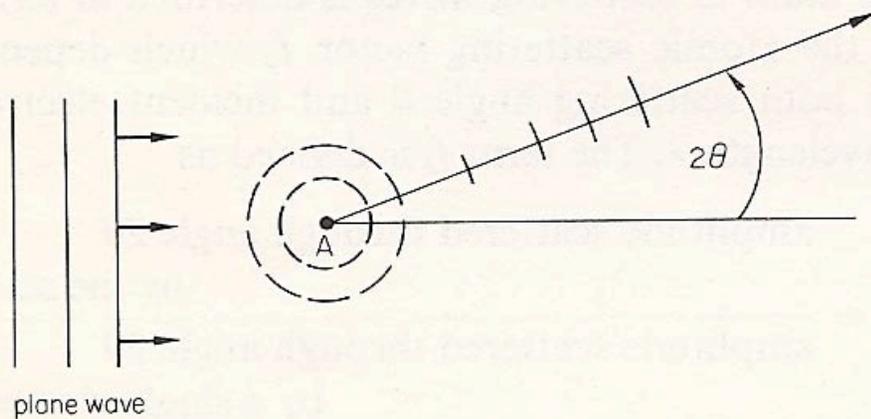


Figure 2.2 The scattering of a plane wave at an atom A through the formation of spherical wavelets travelling at an angle 2θ to the original direction of motion

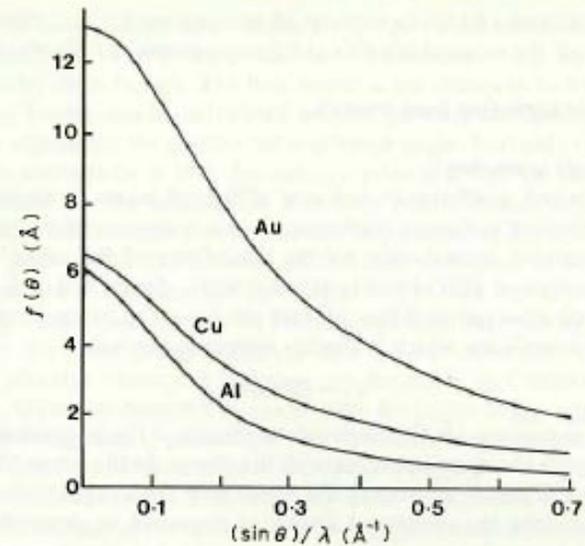


Fig. 2.2 Relationship between the atomic scattering factor $f(\theta)$ (in \AA) and the scattering angle $(\sin \theta) / \lambda$ (in \AA^{-1}) for aluminium, copper and gold calculated using equation (2.1).

Scattering from an isolated atom in free space

Elastic Scattering

Single Atoms:

$$I(\theta) \sim |f(\theta)|^2 = |f_0|^2 \bullet \frac{1}{(\theta^2 + \theta_0^2)^2}$$

$$\theta_0 = \frac{1}{2\pi(0.885a_0Z^{-1/3})}$$

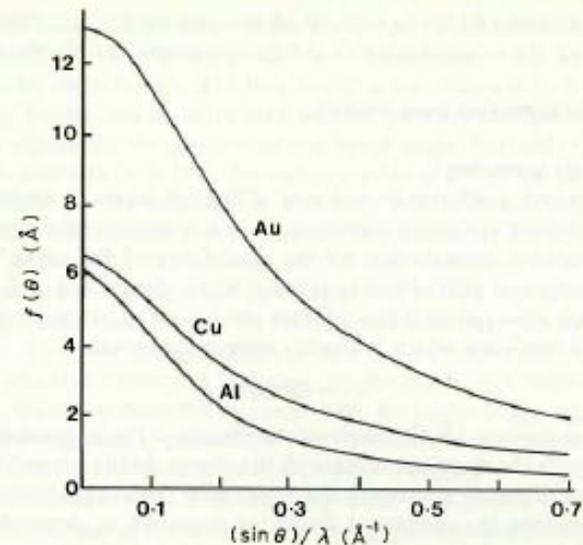


Fig. 2.2 Relationship between the atomic scattering factor $f(\theta)$ (in Å) and the scattering angle $(\sin \theta)/\lambda$ (in Å⁻¹) for aluminium, copper and gold calculated using equation (2.1).

Scattering from an collection of an amorphous collection of atoms
 - neighboring atoms give rise to interference

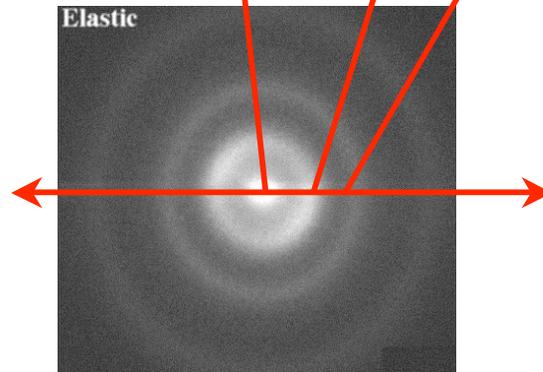
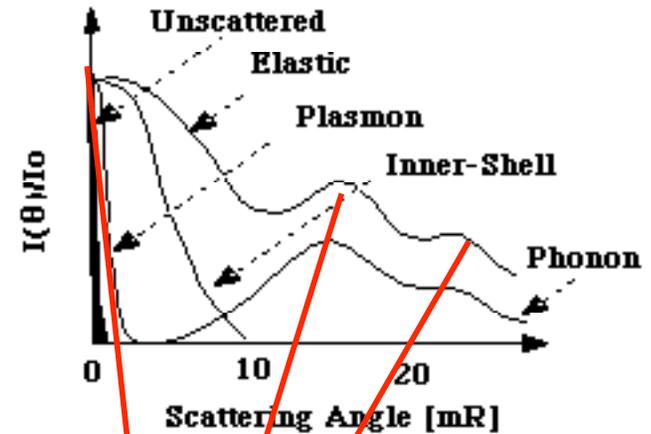
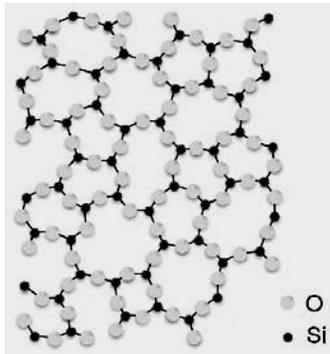
Amorphous Solids:

$$I(\theta) \sim |f(\theta)|^2 \cdot \left| 1 + \frac{\sin(kR)}{kR} \right|$$

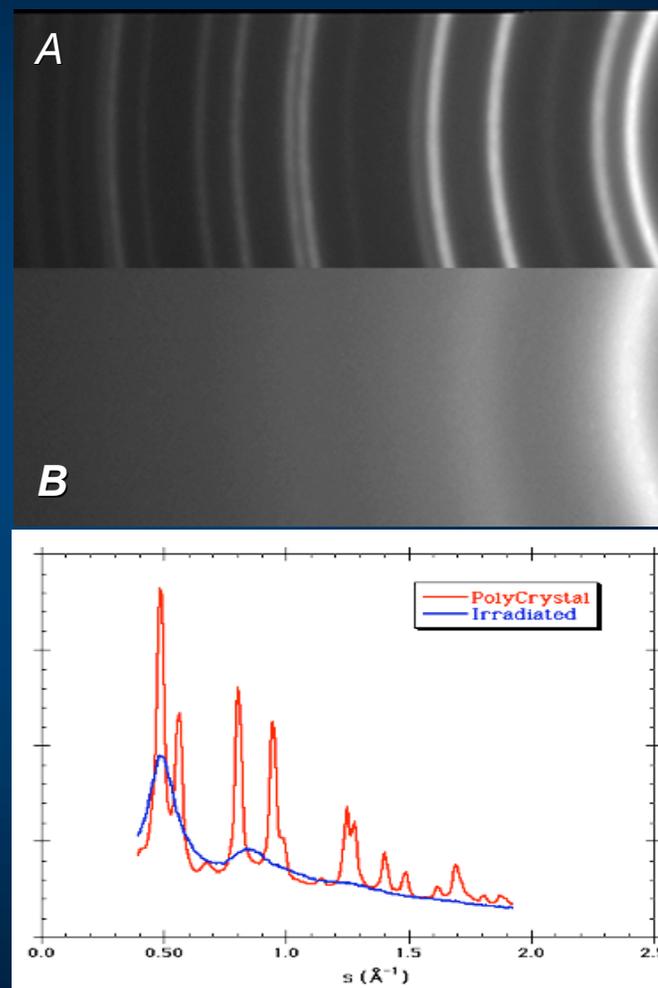
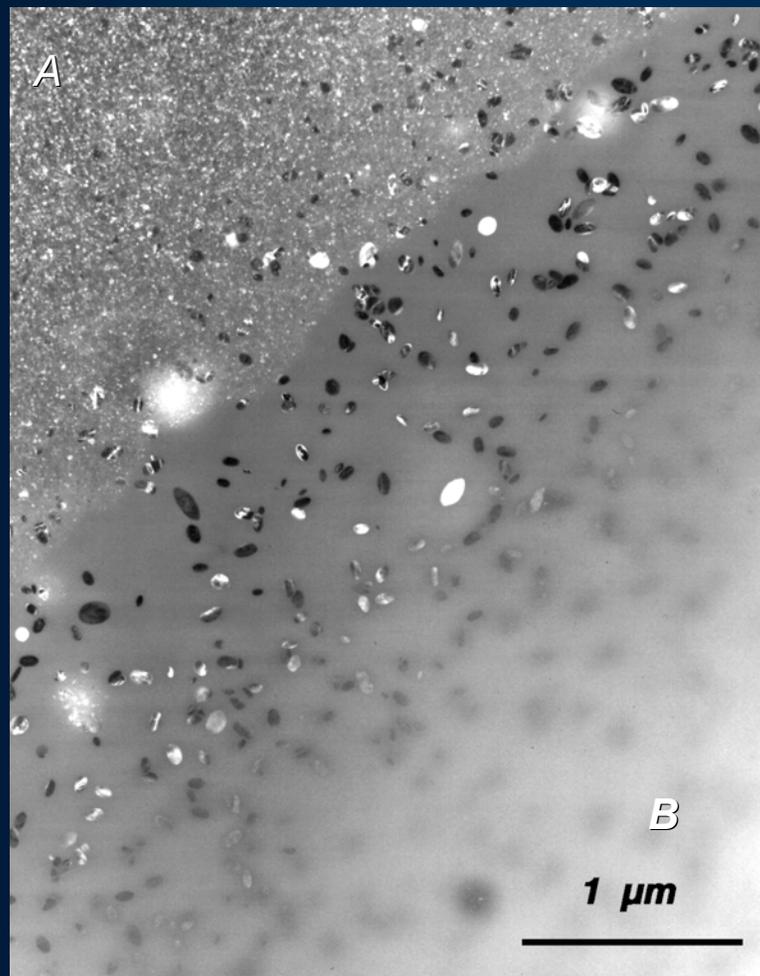
$$k = \frac{4\pi}{\lambda} \sin(\theta)$$

R = Average Interatomic Spacing

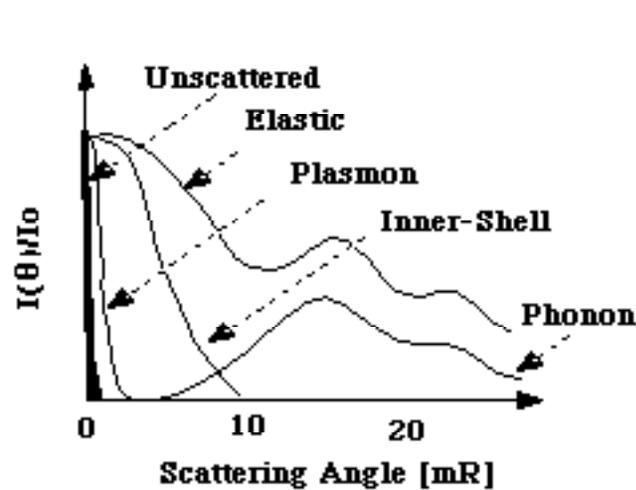
Amorphous
Silica (SiO_2)



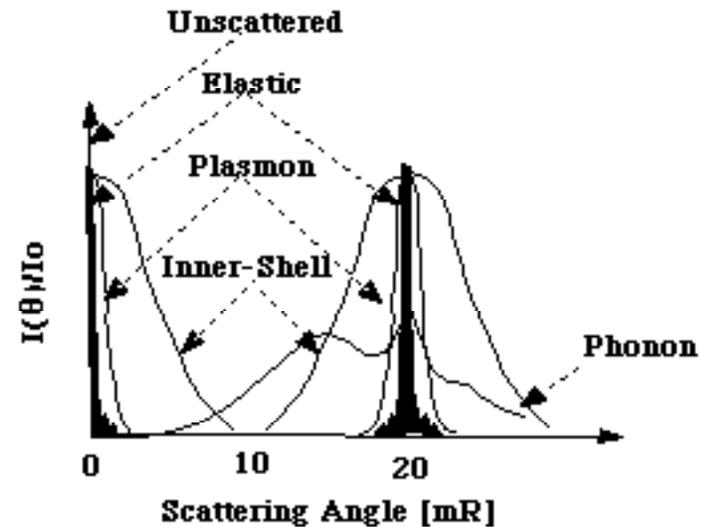
Solid State Order/DisOrder/Amorphization/ Studies



Type of Electron Scattering	Angular Range	Energy Loss
Unscattered	0	0
Elastic	10's-100's mR	~0
Phonon	10's-100's mR	<.025 eV
Inelastic	10's mR	everything else

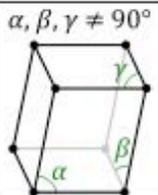
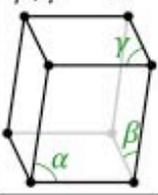
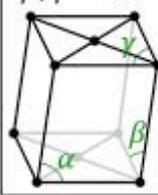
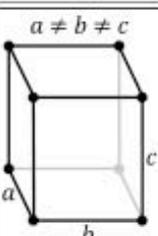
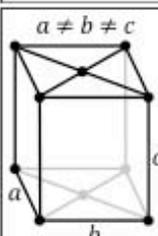
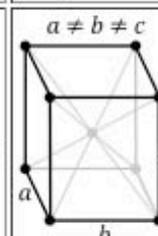
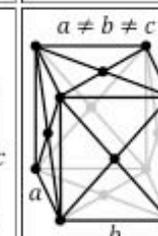
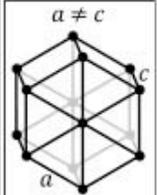
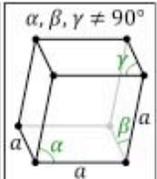
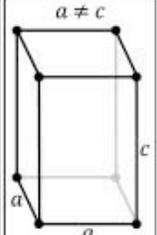
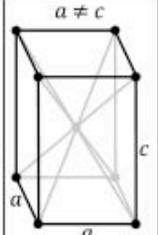
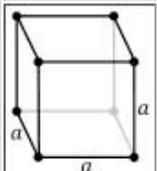
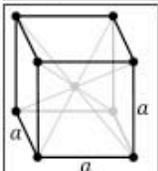
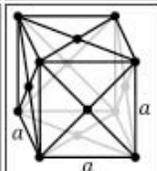


Amorphous Solids



Crystalline Solids

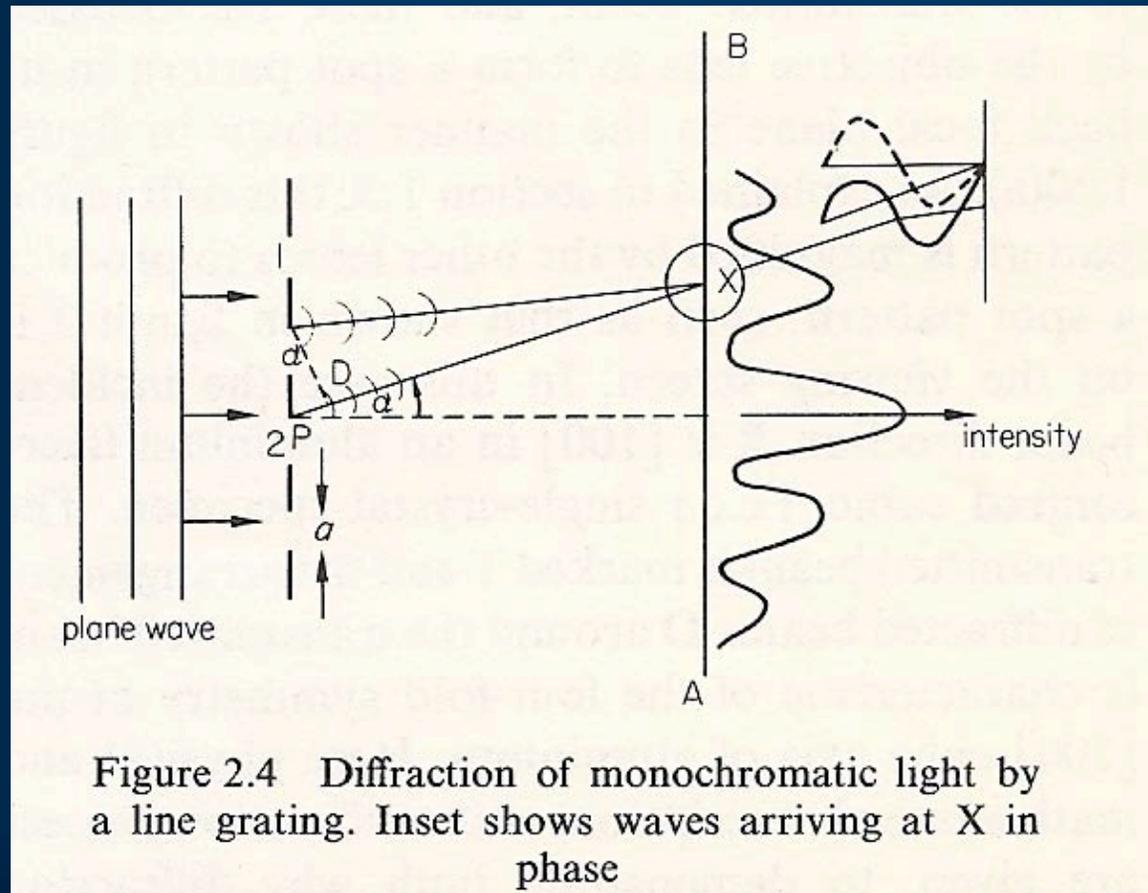
14 Bravais Lattices in 7 Crystal Systems

Crystal system (Defining Symmetry)	Lattices:			
triclinic (none)	$\alpha, \beta, \gamma \neq 90^\circ$ 			
monoclinic (1 diad)	simple	base-centered		
	$\alpha \neq 90^\circ$ $\beta, \gamma = 90^\circ$ 	$\alpha \neq 90^\circ$ $\beta, \gamma = 90^\circ$ 		
orthorhombic (3 perpendicular diads)	simple	base-centered	body-centered	face-centered
	$a \neq b \neq c$			
				
				
				
				
hexagonal (1 hexad)	$a \neq c$ 			
	rhombohedral (1 triad)			
$\alpha, \beta, \gamma \neq 90^\circ$ 				
tetragonal (1 tetrad)	simple	body-centered		
	$a \neq c$ 			
				
cubic (4 triads)	simple	body-centered	face-centered	
	$a = a = a$			
				
				
				

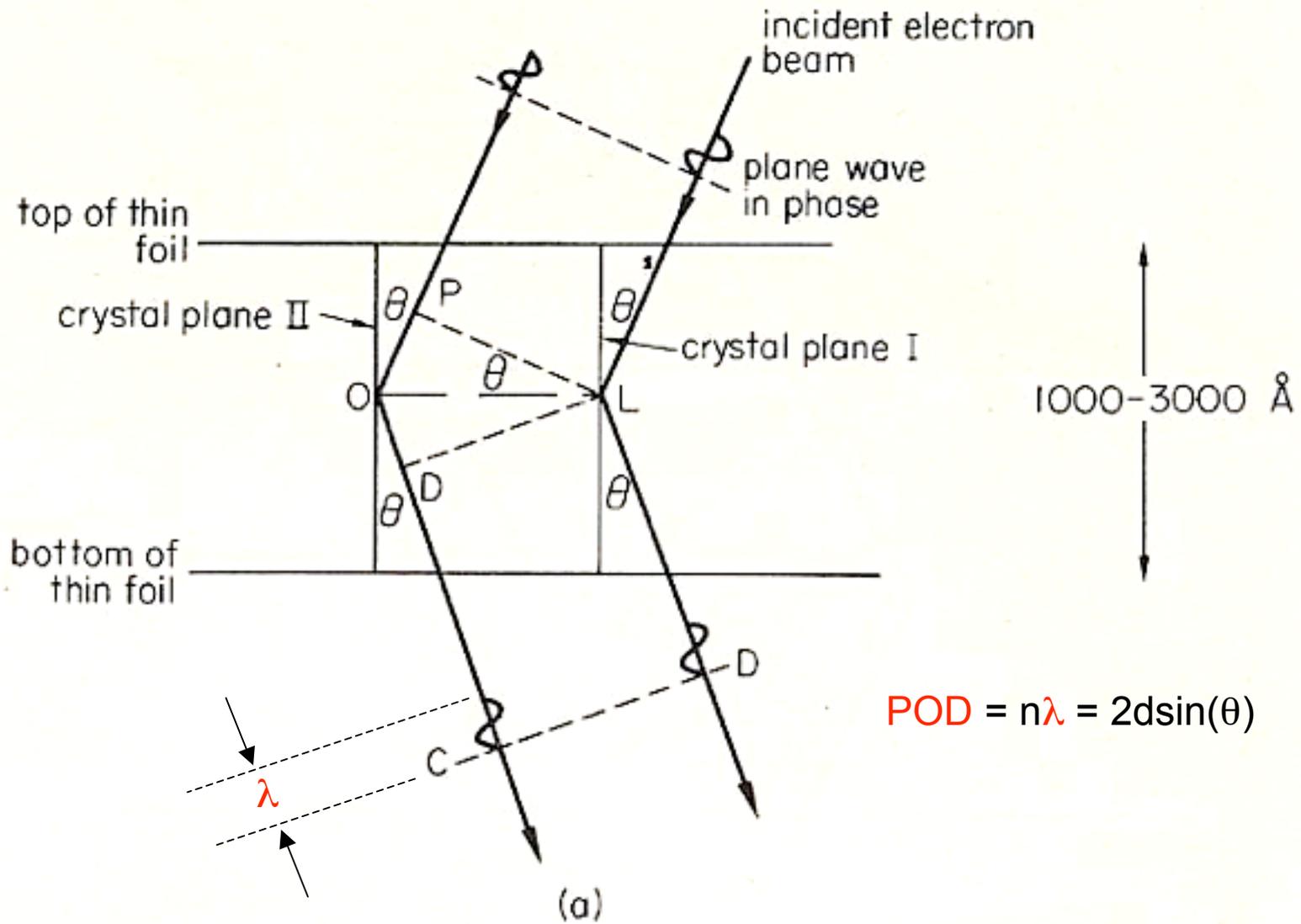
Seven Crystal Systems

Crystal system	Interplanar spacing of the (hkl) plane
cubic $a = b = c$ $\alpha = \beta = \gamma = 90^\circ$	$\frac{1}{d^2} = \frac{1}{a^2} (h^2 + k^2 + l^2)$
tetragonal $a = b \neq c$ $\alpha = \beta = \gamma = 90^\circ$	$\frac{1}{d^2} = \frac{1}{a^2} (h^2 + k^2) + \frac{1}{c^2} l^2$
orthorhombic $a \neq b \neq c$ $\alpha = \beta = \gamma = 90^\circ$	$\frac{1}{d^2} = \frac{1}{a^2} h^2 + \frac{1}{b^2} k^2 + \frac{1}{c^2} l^2$
hexagonal $a = b \neq c$ $\alpha = \beta = 90^\circ; \gamma = 120^\circ$	$\frac{1}{d^2} = \frac{4}{3a^2} (h^2 + hk + k^2) + \frac{1}{c^2} l^2$
rhombohedral $a = b = c$ $\alpha = \beta = \gamma < 120^\circ \neq 90^\circ$	$\frac{1}{d^2} = \frac{1}{a^2} \frac{(1 + \cos \alpha) \{ (h^2 + k^2 + l^2) - (1 - \tan^2 \frac{1}{2} \alpha) (hk + kl + lh) \}}{1 + \cos \alpha - 2 \cos^2 \alpha}$
monoclinic $a \neq b \neq c$ $\alpha = \gamma = 90^\circ \neq \beta$	$\frac{1}{d^2} = \frac{1}{a^2} \frac{h^2}{\sin^2 \beta} + \frac{1}{b^2} k^2 + \frac{1}{c^2} \frac{l^2}{\sin^2 \beta} - \frac{2hl \cos \beta}{ac \sin^2 \beta}$
triclinic $a \neq b \neq c$ $\alpha \neq \beta \neq \gamma$	$\frac{1}{d^2} = \frac{1}{V^2} (s_{11}h^2 + s_{22}k^2 + s_{33}l^2 + 2s_{12}hk + 2s_{23}kl + 2s_{33}lh)$ <p>where</p> $V^2 = a^2b^2c^2(1 - \cos^2 \alpha - \cos^2 \beta - \cos^2 \gamma + 2 \cos \alpha \cos \beta \cos \gamma)$ <p>and</p> $s_{11} = b^2c^2 \sin^2 \alpha$ $s_{22} = a^2c^2 \sin^2 \beta$ $s_{33} = a^2b^2 \sin^2 \gamma$ $s_{12} = abc^2(\cos \alpha \cos \beta - \cos \gamma)$ $s_{23} = a^2bc(\cos \beta \cos \gamma - \cos \alpha)$ $s_{31} = ab^2c(\cos \gamma \cos \alpha - \cos \beta)$

Periodic Structures Create Constructive/Destructive Interference



Simple Geometrical Description of Bragg's Law

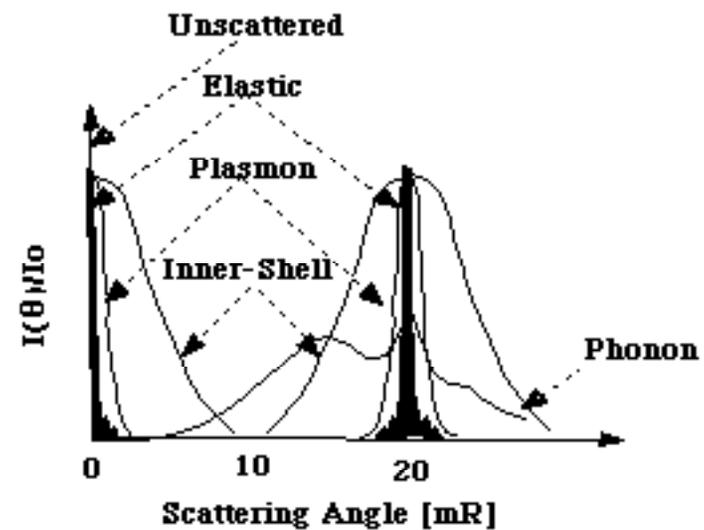


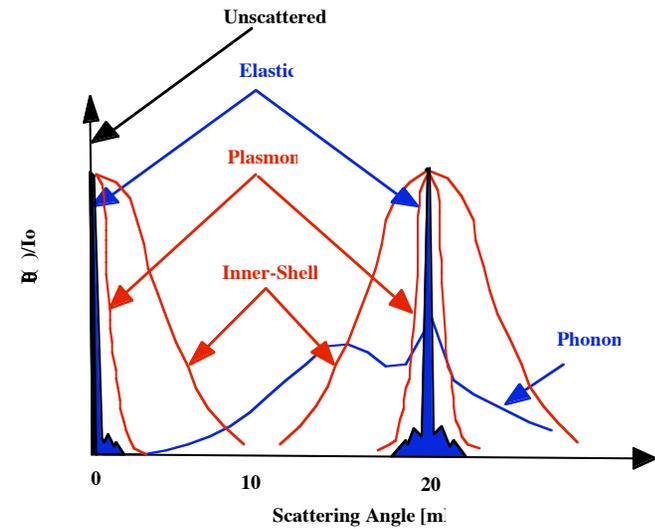
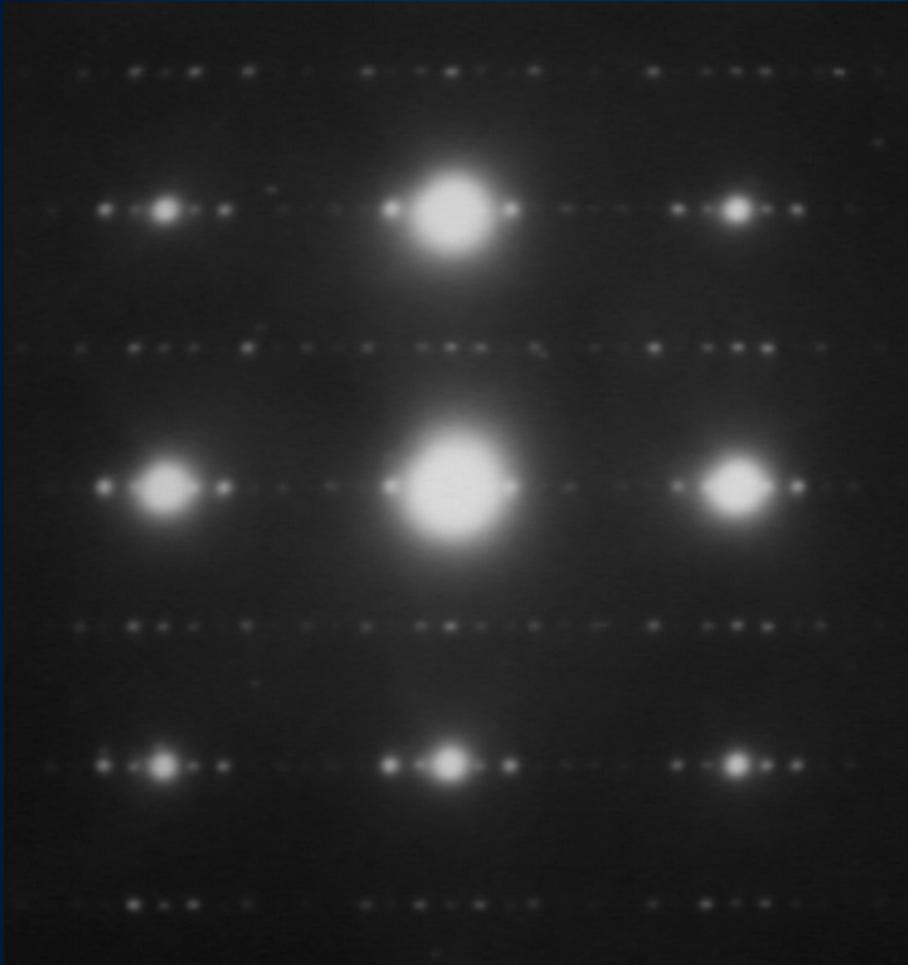
Elastic Scattering

Crystalline Solids:

$$I(\theta) \sim |F(\mathbf{hk}l)|^2$$

$$F(\mathbf{hk}l) = \sum_j f_j(\theta) e^{(-2\pi i \mathbf{k} \cdot \vec{r}_j)}$$





Elastic Scattering : Crystalline Solids

$$I(\theta) \sim |F(\mathbf{hkl})|^2$$

$$F(\mathbf{hkl}) = \sum_j f_j(\theta) \exp(-2\pi i \vec{g} \cdot \vec{r}_j)$$

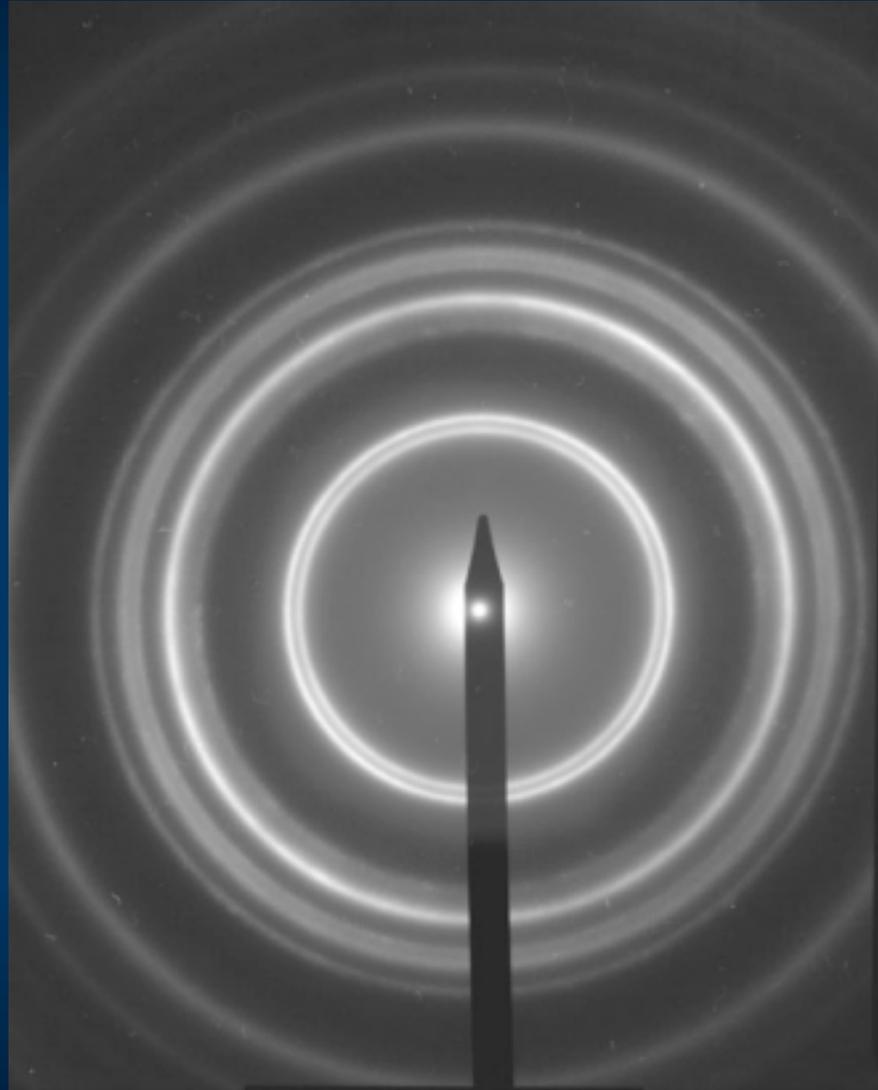
$$V(\mathbf{r}) = - \sum_{\vec{g}} V_{\vec{g}} \exp(2\pi i \vec{g} \cdot \vec{r}) ; \quad V_{\vec{g}} = \frac{h^2}{2\pi m V_e} f(\theta)$$

Type of Diffraction Patterns

- Electron diffraction patterns produced in transmission in the electron microscope can be of three different types.
 - (a) Ring pattern Polycrystalline, and amorphous specimen
 - (b) Spot pattern Single-crystal region of the specimen
 - (c) Kikuchi line pattern
- Type (b) and (c) often occur on the same diffraction pattern. In general, spot and Kikuchi patterns will be taken from a specific area of the specimen and are known as 'selected area' diffraction patterns (SADPs).

Ring Pattern:

- The major use of ring patterns is in the identification of phases using extraction replicas. These diffraction patterns also arise from very fine grain size polycrystalline material such as physically or chemically vapor deposited or electrodeposited thin foils.



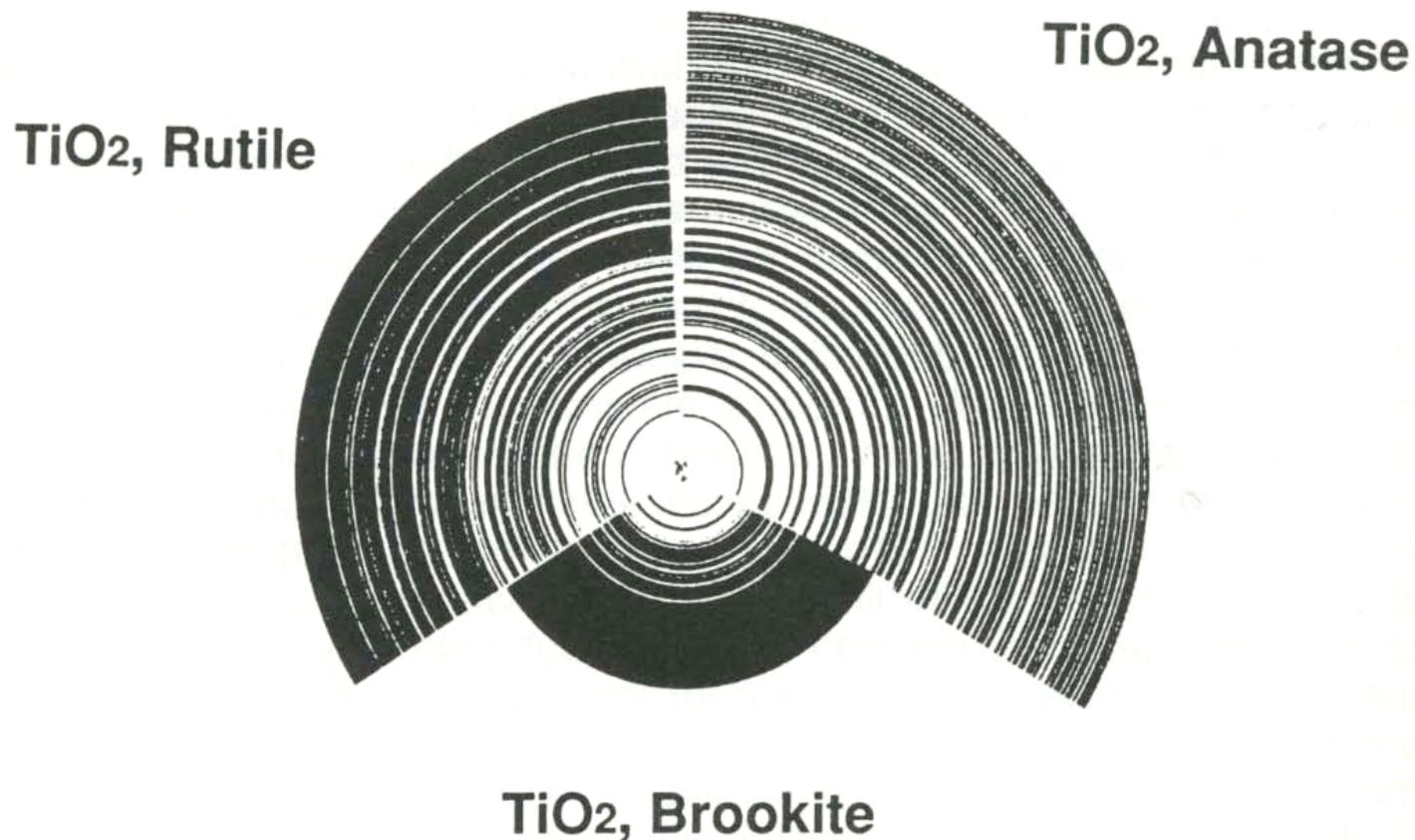
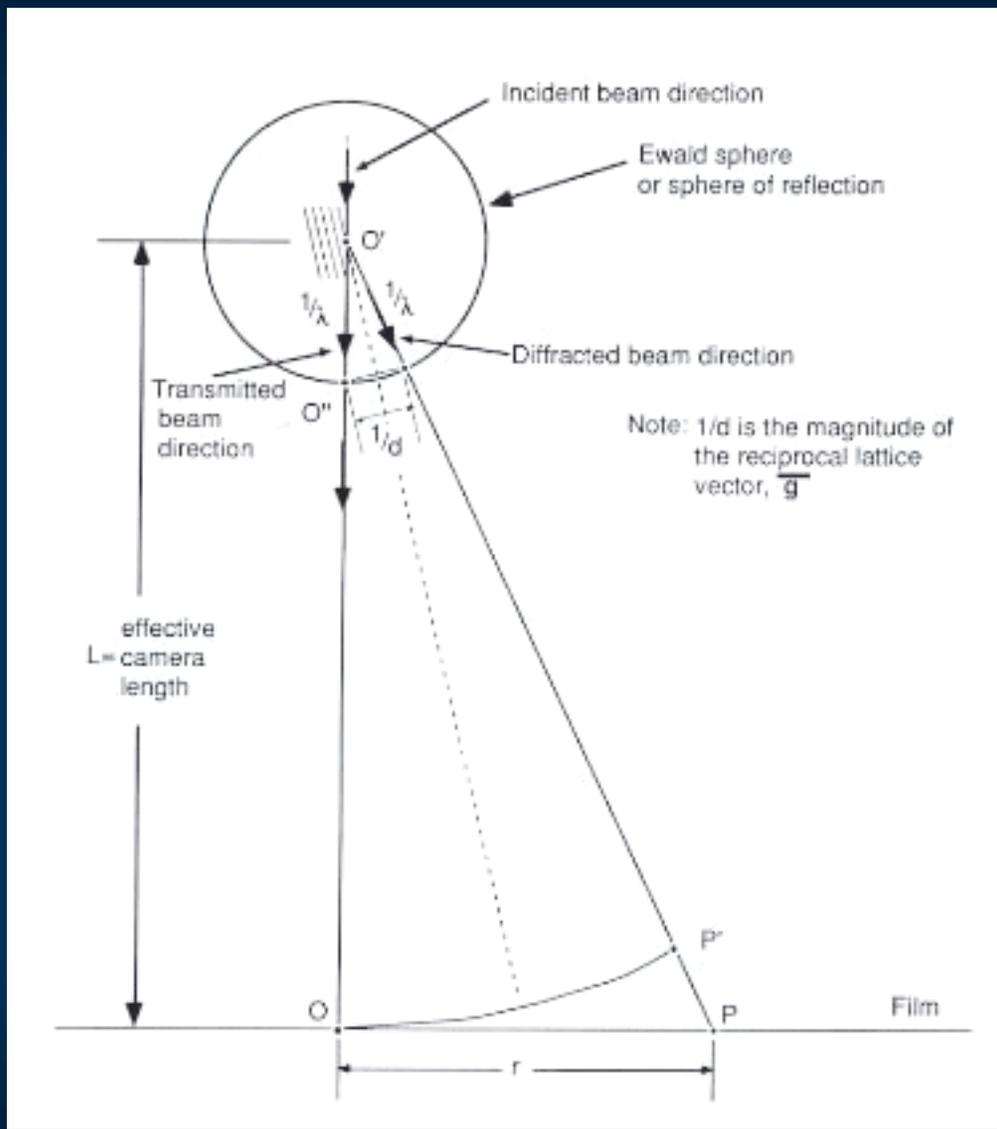


Figure 5.10. Sections of ring patterns of the three phases of TiO₂ (rutile, brookite, and anatase) showing that the largest d-spacings (smallest r-spacings) are the most diagnostic for identifying these compounds.



Ring pattern: what can we obtain

- d-spacing

$$Rd_{hkl} = L\lambda$$

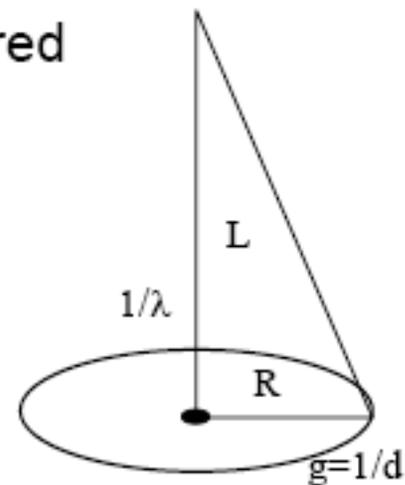
R: the measured ring radius

d_{hkl} : the d-spacing being measured

L: camera length

λ : wave length of electron beam

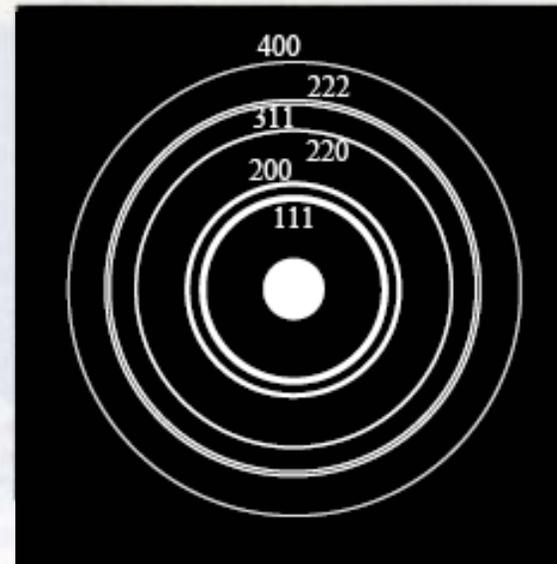
- Camera length calibration
- Crystalline / particle fineness



$$Rd_{hkl} = \lambda L$$

$$\lambda_{rel} = \frac{h}{mv} = \frac{h}{m_0v} \sqrt{1 - \gamma^2}$$

$$= \frac{12.27}{\sqrt{V_a}} [1 + 0.978 \times 10^{-6} V_a]^{-1/2}$$



Use the cubic interplanar spacing formula

$$d_{hkl} = \frac{a}{\sqrt{h^2 + k^2 + l^2}}, \quad a = 0.40497 \text{ nm}$$

to calculate the d-spacings below for the first five reflections of aluminum:

<u>r-distance</u>	<u>hkl</u>	<u>d-spacing</u>	<u>λ</u>
10.3 mm	111	0.2338 nm	2.408 nm-mm
11.9	200	0.2025	2.409
16.8	220	0.1432	2.406
19.7	311	0.1221	2.405
20.6	222	0.1169	2.408

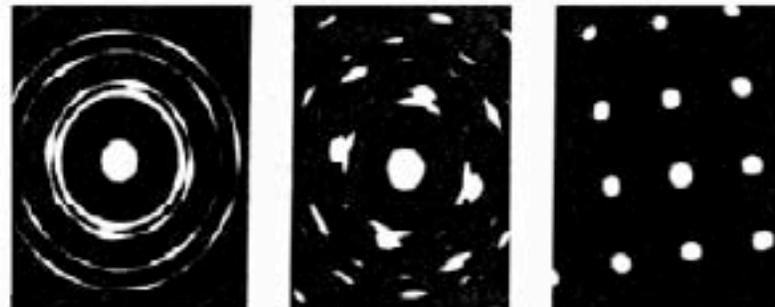
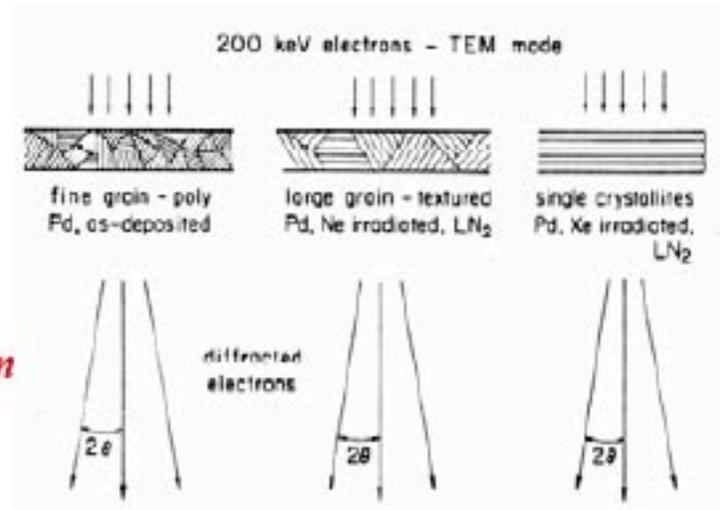
Average = 2.407 nm-mm

Electron Properties as a Function of Accelerating Voltage

Table 1.2. Electron Properties as a Function of Accelerating Voltage

Accelerating voltage (kV)	Nonrelativistic wavelength (nm)	Relativistic wavelength (nm)	Mass ($\times m_0$)	Velocity ($\times 10^8$ m/s)
100	0.00386	0.00370	1.196	1.644
120	0.00352	0.00335	1.235	1.759
200	0.00273	0.00251	1.391	2.086
300	0.00223	0.00197	1.587	2.330
400	0.00193	0.00164	1.783	2.484
1000	0.00122	0.00087	2.957	2.823

*Electron Beam
Diffraction of a Pd film*



Indexing Diffraction patterns

The Ring Patterns

The radius of each ring is characteristic of the spacing of the reflecting planes in the crystal and the magnification settings of the microscope lenses.

Procedure for indexing ring patterns is as follows:

1. When the identity of the material is known, we have the following:
 - Measure the ring diameters.
 - Determine the ratios of the squares of the diameters of the outer rings to that of the first or second (low-index) ring.
 - Check the ratios against a table of ratios of the interplanar spacings for the crystal structure of interest, see table 2.2.
2. When the identity of the substance is unknown, we have the following:
 - Measure the diameter of the rings.
 - Convert the distances into interplanar spacings using the camera constant defined as $Rd = \lambda L$.
 - Use ASTM (American Society for Testing Materials) index to identify the phase, starting with the most likely on the basis of the known constituents of the alloy.

Diffraction patterns from polycrystalline specimens are most commonly used either to calibrate the camera length or to identify precipitates.

Table 2.2 Proportionalities of the ratios of the radii of ring patterns for different crystal structures

Crystal structure	Formula for interplanar spacing	Possible values of h, k, l for reflection (up to 20)	Criterion
simple cubic	$\frac{1}{d^2} = \frac{h^2 + k^2 + l^2}{a^2} = \frac{N}{a^2}$	N an integer except 7 or 15	ratios of squares of radii $\propto N$
f.c.c.	$\frac{1}{d^2} = \frac{h^2 + k^2 + l^2}{a^2} = \frac{N}{a^2}$	$N = 3, 4, 8, 11, 12, 16, 19, 20$	ratios $\propto N$
b.c.c.	$\frac{1}{d^2} = \frac{h^2 + k^2 + l^2}{a^2} = \frac{N}{a^2}$	$N = 2, 4, 6, 8, 10, 12, 14, 16, 18, 20$	ratios $\propto N$
diamond structure	$\frac{1}{d^2} = \frac{h^2 + k^2 + l^2}{a^2} = \frac{N}{a^2}$	$N = 2, 8, 11, 16, 19$	ratios $\propto N$
tetragonal	$\frac{1}{d^2} = \frac{h^2 + k^2}{a^2} + \frac{l^2}{c^2}$	$h^2 + k^2 = 1, 2, 4, 5, 8, 9, 10, 13, 16, 17, 18, 20$	ratios frequently proportional to 2; use Bunn chart, see Henry <i>et al.</i> (1951)
hexagonal	$\frac{1}{d^2} = \frac{4h^2 + hk + k^2}{3a^2} + \frac{l^2}{c^2}$	$h^2 + hk + l^2 = 1, 3, 4, 7, 9, 12, 13, 16, 19$	ratios frequently proportional to 3; use Bunn chart, see Henry <i>et al.</i> (1951)

Table A4.1 Occurrence of reflections for the cubic crystal structures

Line no. $N = h^2 + k^2 + l^2$	hkl indices	$N^{1/2} = (h^2 + k^2 + l^2)^{1/2}$	f.c.c. diamond			Line no. $N = h^2 + k^2 + l^2$	hkl indices	$N^{1/2} = (h^2 + k^2 + l^2)^{1/2}$	b.c.c.	f.c.c.	diamond
1	100	1.00				33	522, 441	5.745			
2	110	1.414	×			34	530, 433	5.831	×		
3	111	1.732		×	×	35	531	5.916		×	×
4	200	2.00	×	×	×	36	600, 442	6.00	×	×	×
5	210	2.236				37	610	6.083			
6	211	2.450	×			38	611, 532	6.164	×		
7	—	—				39	—	—			
8	220	2.828	×	×	×	40	620	6.325	×	×	×
9	300, 221	3.00				41	621, 540, 443	6.403			
10	310	3.162	×			42	541	6.481	×		
11	311	3.317		×	×	43	533	6.557		×	×
12	222	3.464	×	×		44	622	6.633	×	×	×
13	320	3.606				45	630, 542	6.708			
14	321	3.742	×			46	631	6.782	×		
15	—	—				47	—	—			
16	400	4.00	×	×	×	48	444	6.928	×	×	
17	410, 322	4.123				49	700, 632	7.00			
18	411, 330	4.243	×			50	710, 550, 543	7.071	×		
19	331	4.359		×	×	51	711, 551	7.141		×	×
20	420	4.472	×	×	×	52	640	7.211	×	×	
21	421	4.583				53	720, 641	7.280			
22	332	4.690	×			54	721, 633, 552	7.349	×		
23	—	—				55	—	—			
24	422	4.899	×	×	×	56	642	7.483	×	×	×
25	500, 430	5.00				57	722, 544	7.550			
26	510, 431	5.099	×			58	730	7.616	×		
27	511, 333	5.196		×	×	59	731, 553	7.681		×	×
28	—	—				60	—	—			
29	520, 432	5.385				61	650, 643	7.810			
30	521	5.477	×			62	732, 651	7.874	×		
31	—	—				63	—	—			
32	440	5.657	×	×	×	64	800	8.00	×	×	×

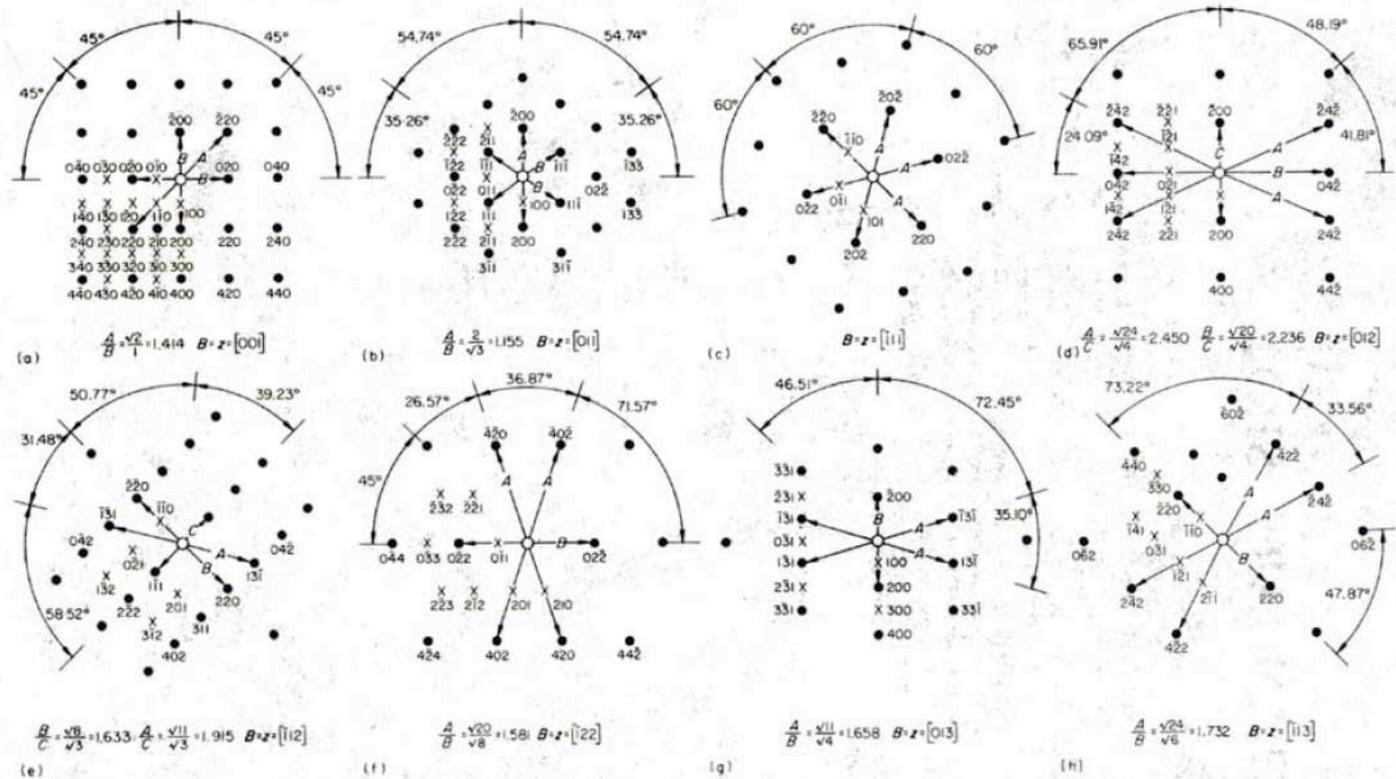
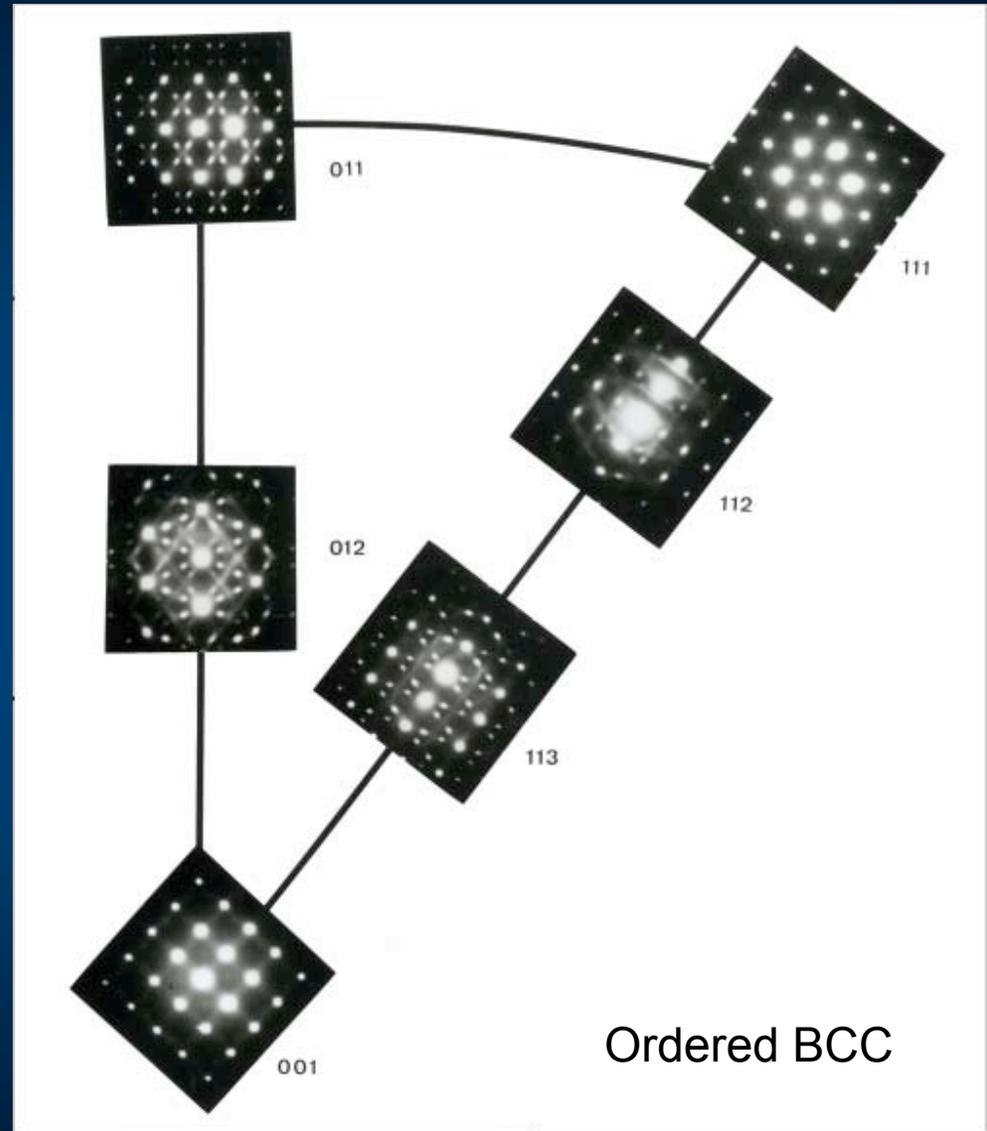
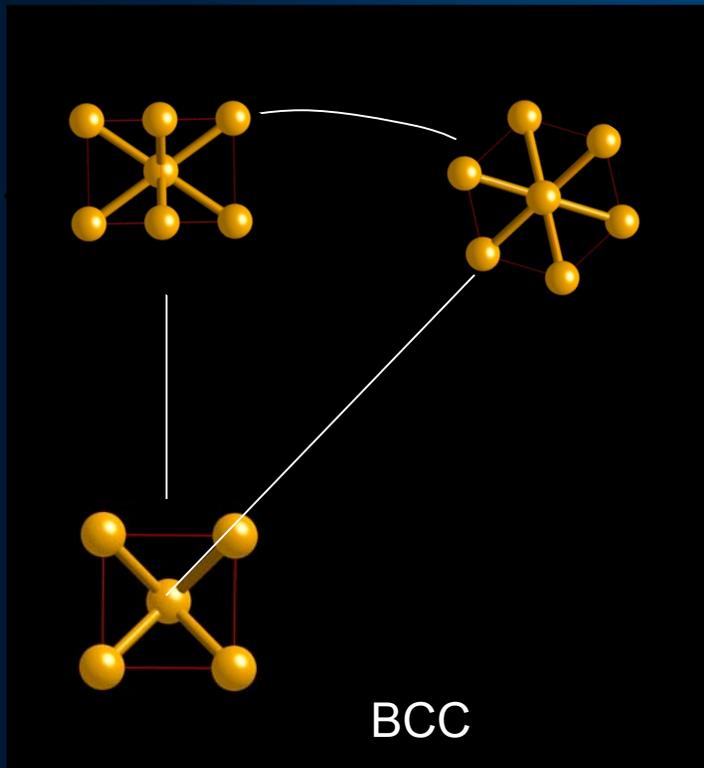
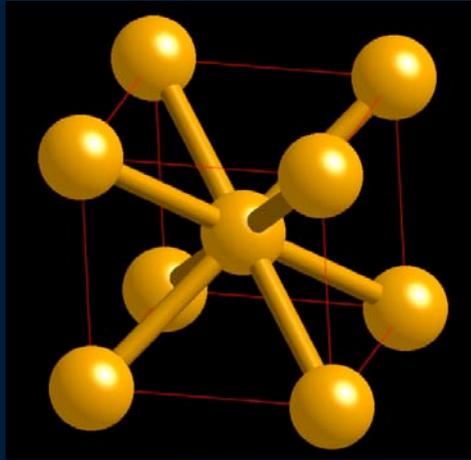


Figure A4.1 Single-crystal spot transmission electron diffraction patterns for the f.c.c. crystal structure ($u^2 + v^2 + w^2 < 22$). The zone axis z , defined in appendix 1, is the beam direction B defined in section 2.7.2, as indicated. The crosses in one quadrant of the diagram indicate the positions of the spots for the ordered f.c.c. ($L1_2$) unit cell. The complete pattern may be generated by repeating these spots in the remainder of the pattern and indexing using the addition of vectors, see section 2.7.2.1

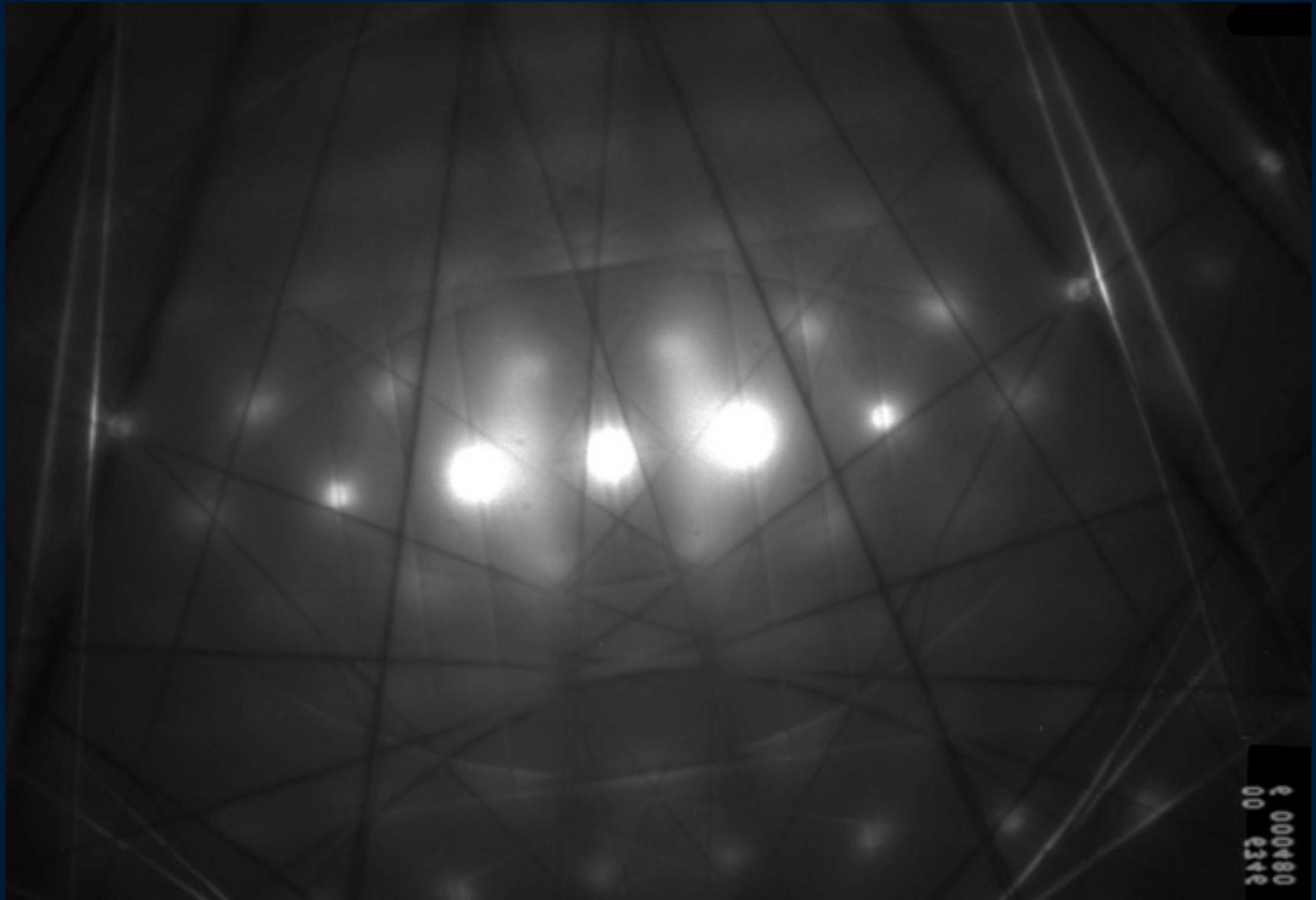


Diffraction Space is related to Real Space

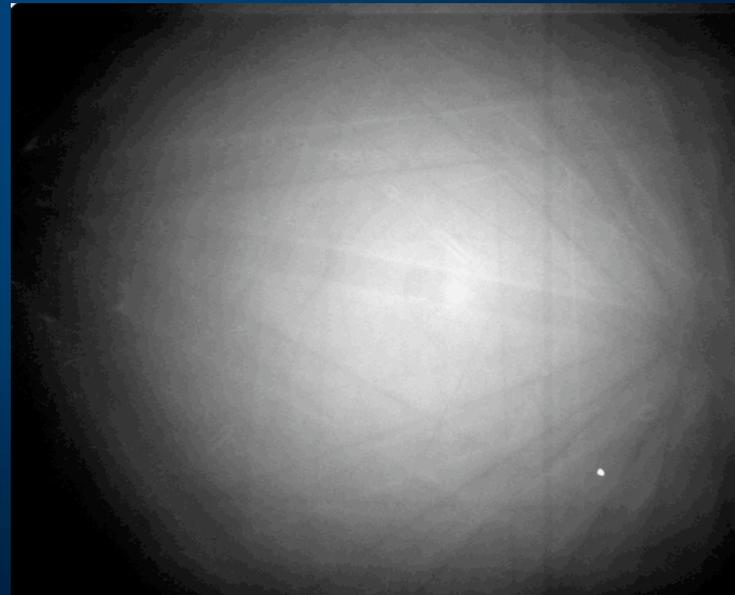
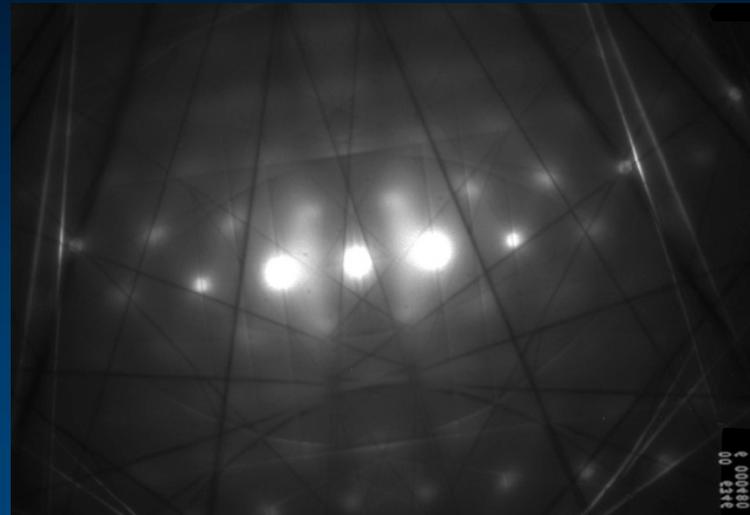
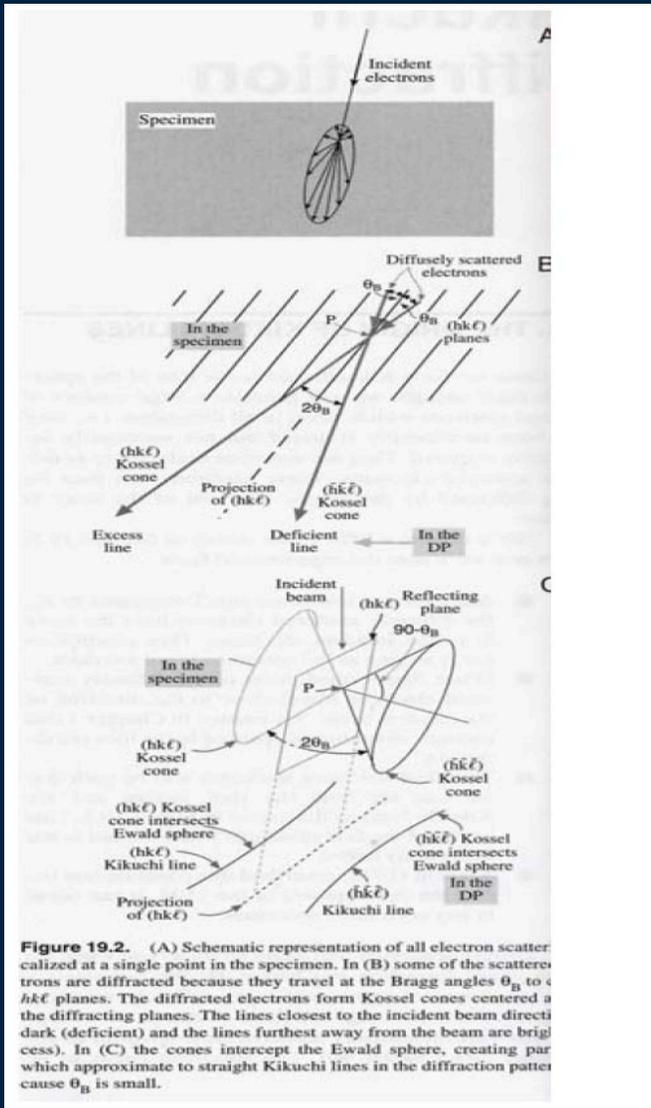
Index Simple Patterns – spots are produced by planes in one zone

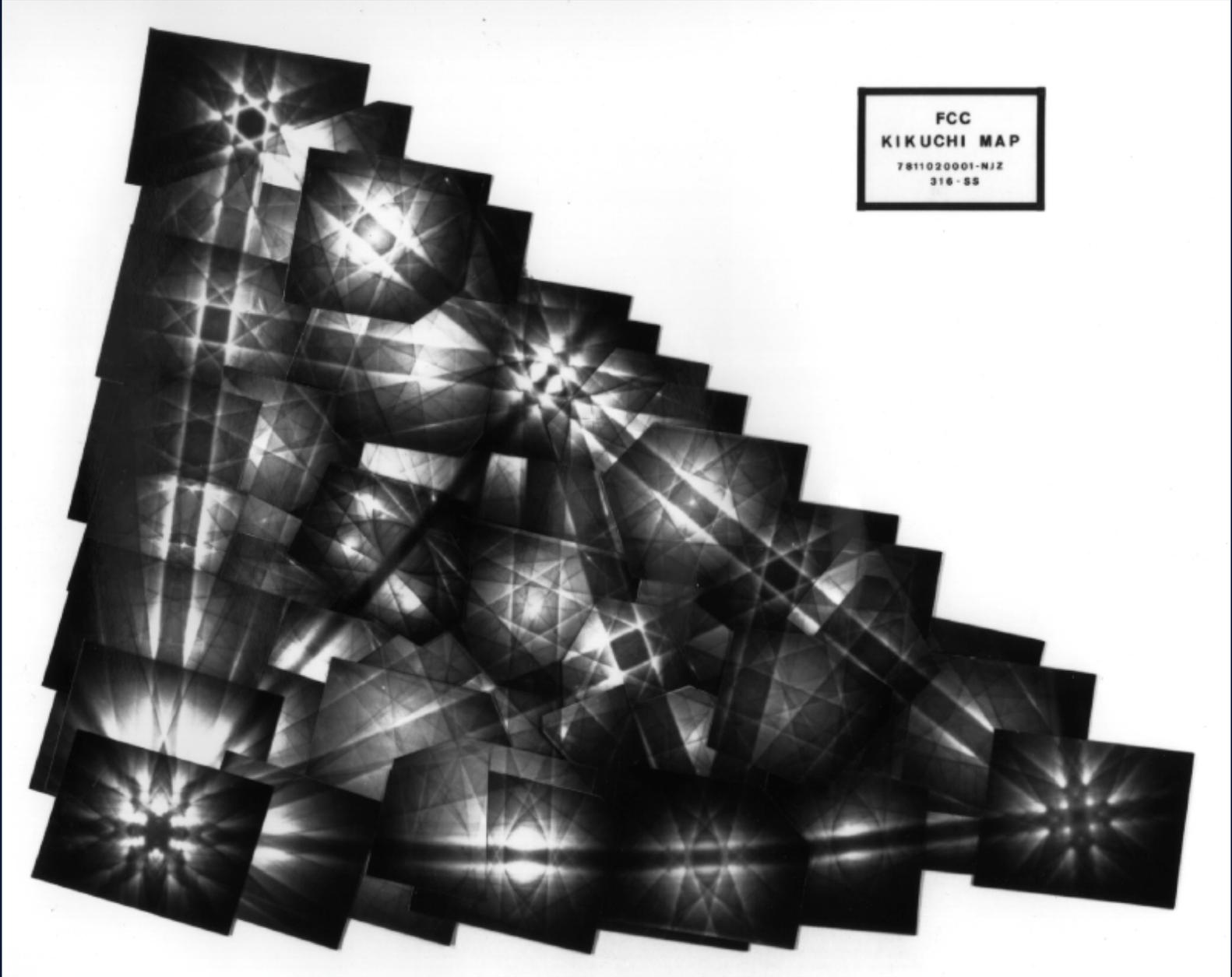
- Frequently these patterns may be easily recognized from their simplicity and their six-, four-, three- and two-fold symmetry.
- (a) *Indexing the pattern.* The indexing procedure involves one of two procedures:
 - (i) Camera constant method – Camera constant known, materials known. Measure the distance R of the spot from the center spot, figure 2.20 (a) (most accurately determined by measuring the total distance between several spots in this direction and dividing as necessary). Divide the camera constant λL ($Rd = \lambda L$) by R and check the result against a list of d spacings.
 - (ii) Method of ratios. Camera constant unknown. Material λL known. Measure distances of spots from center spot relative to that between the nearest spot and the center. Check against tables of ratios of d spacings for low-index planes. Account must be taken of the occurrence of planes with the same d spacing, see table A 4.1.

Kikuchi Lines

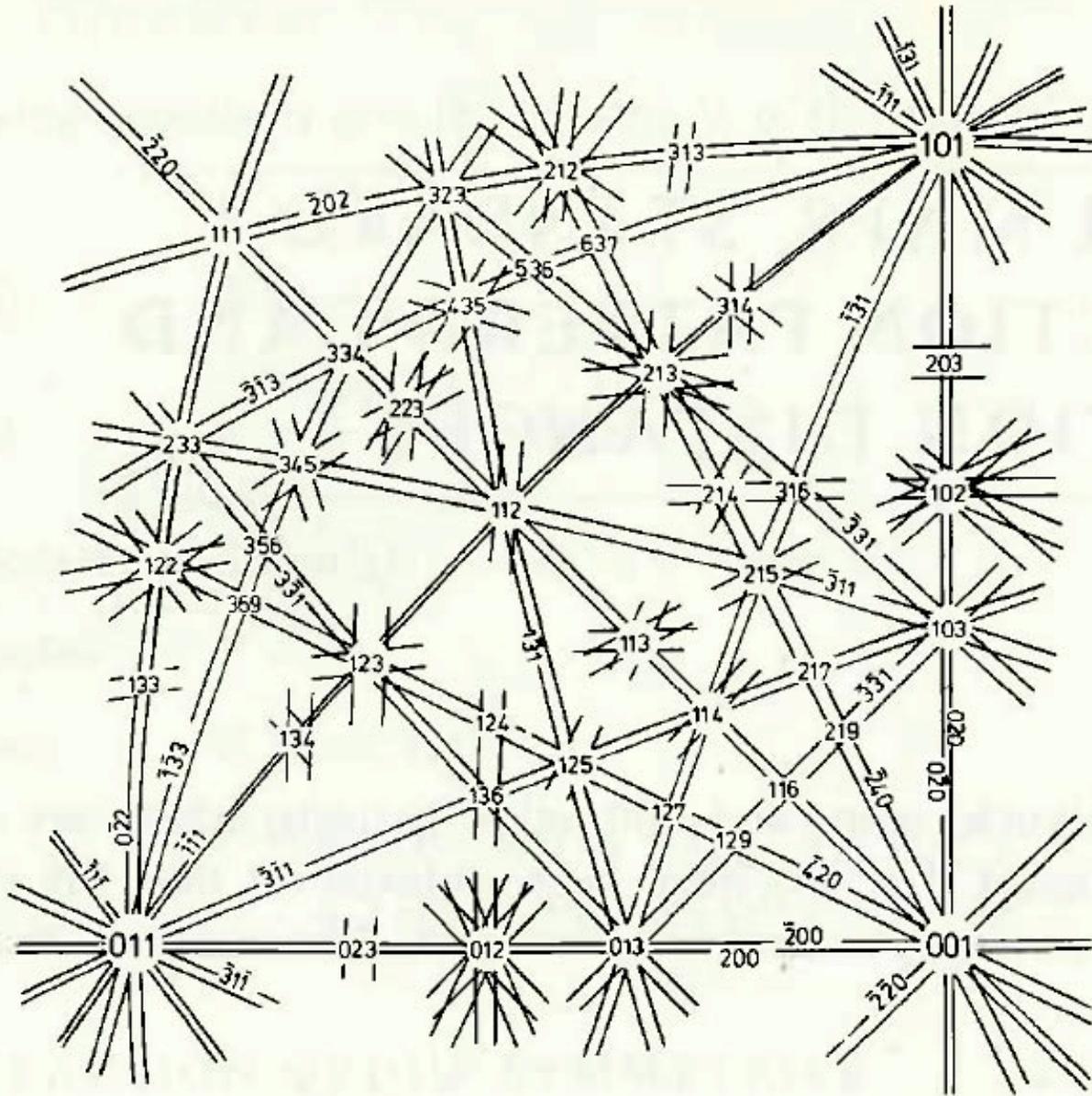


Kikuchi Lines





FCC
KIKUCHI MAP
7811020001-NJZ
316-SS



Specimen Holders

Single-tilt holder
Double-tilt holder
Low-background holder
Heating holder
Cooling holder
Cryo-transfer holder

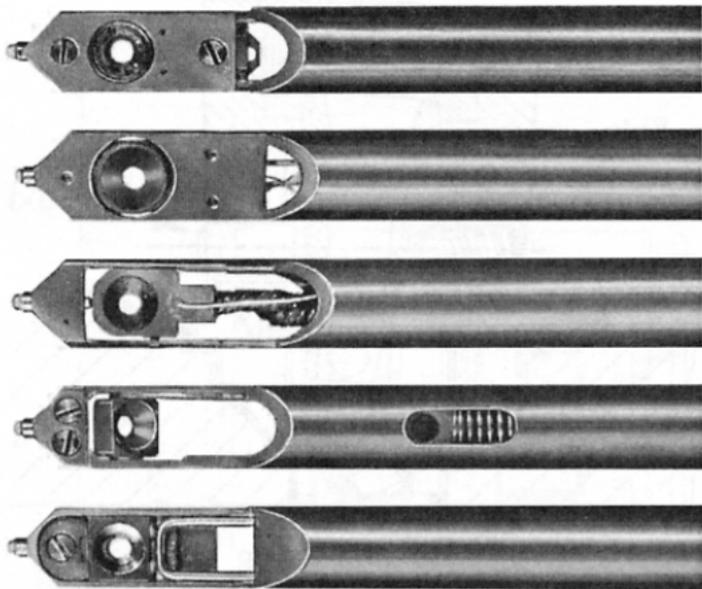


Figure 8.8. Examples of different designs for the side-entry holder. From the top, they are: a rotation holder, a heating holder, a cooling holder, a double-tilt holder, and a single-tilt holder.

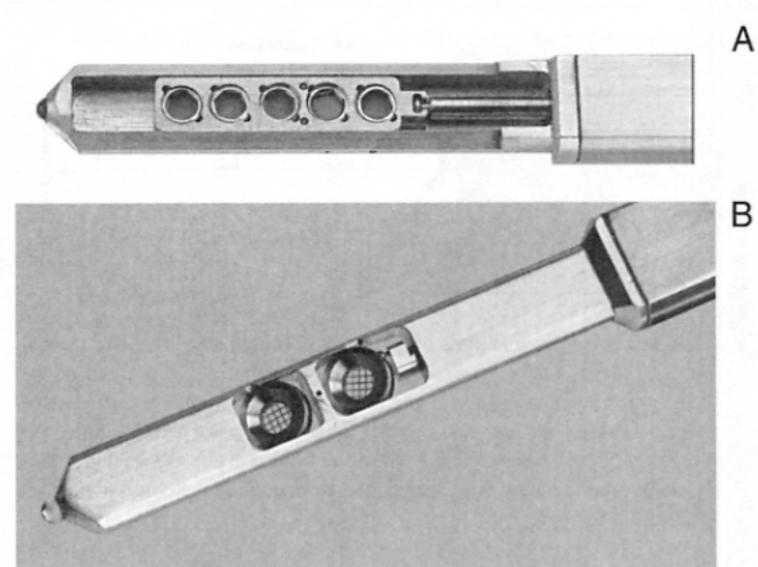


Figure 8.9. Multiple-specimen holders. (A) Five-specimen single-tilt and (B) two-specimen double-tilt.

How do Apertures & Condensor Lens affect Diffraction

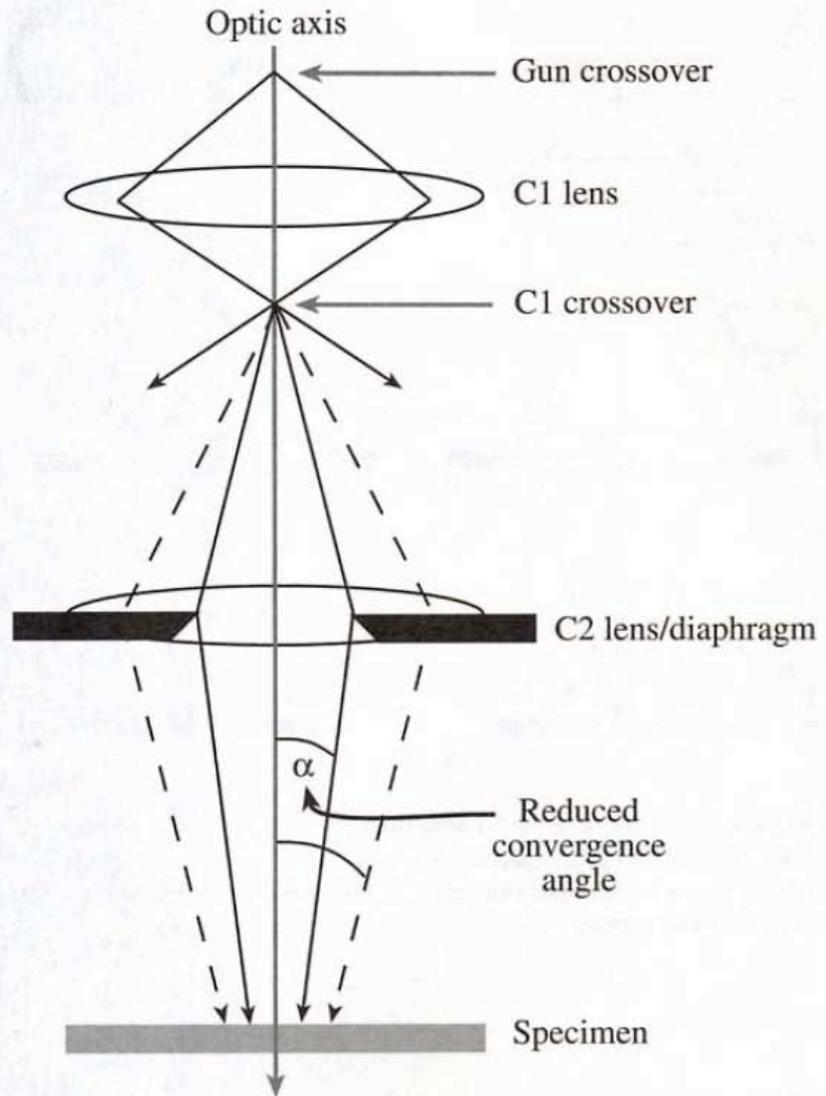


Figure 9.2. Effect of the C2 aperture on the beam coherence: a smaller aperture creates a more parallel, more coherent beam.

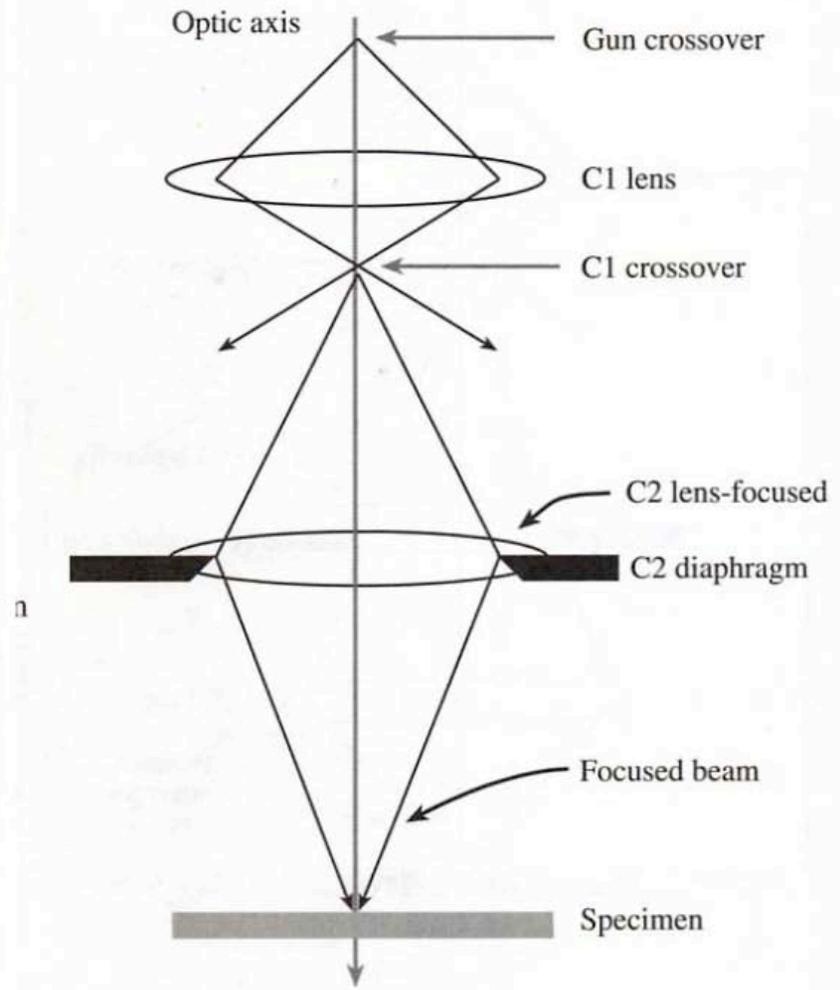
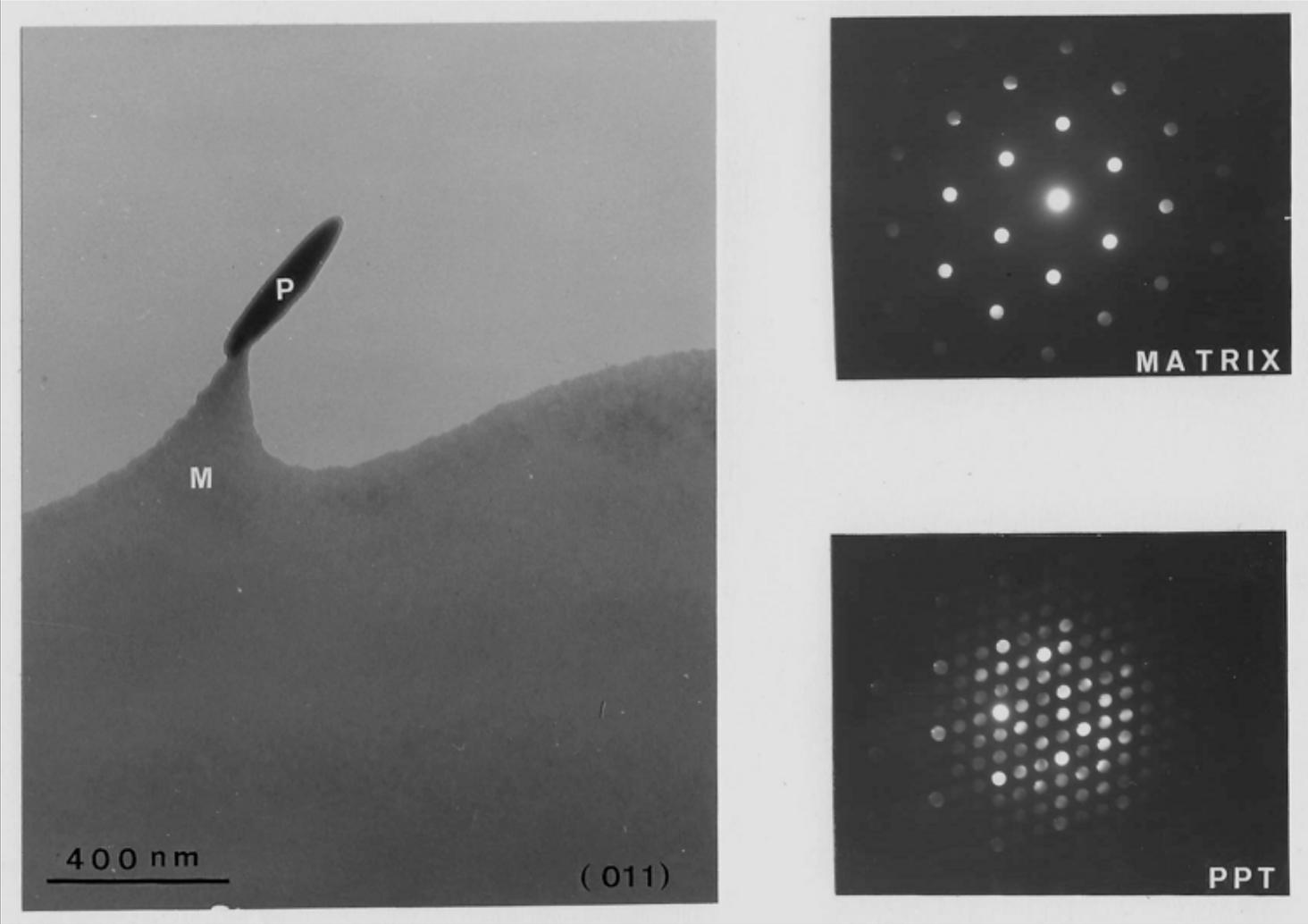
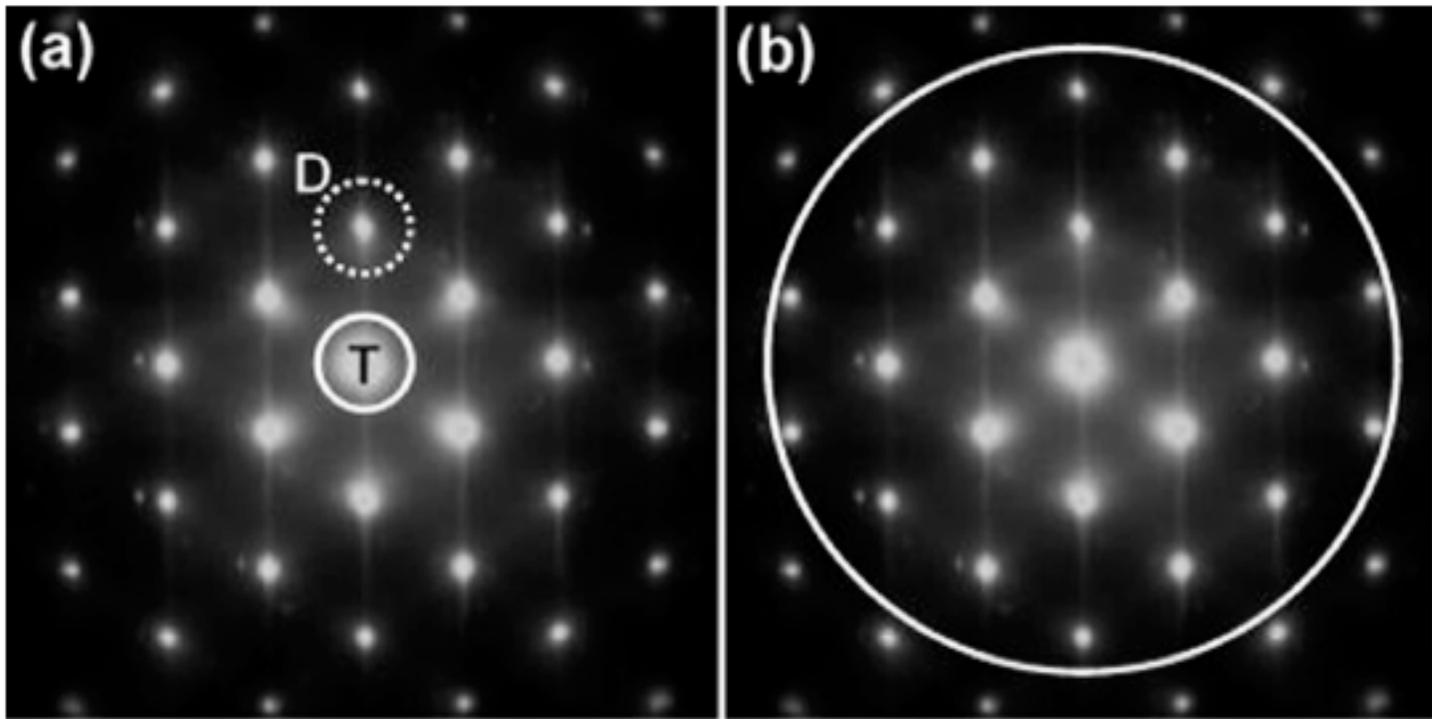


Figure 9.3. A focused C2 lens illuminates a small area of the specimen with a nonparallel beam.

Electron Diffraction





Obtaining ~ Parallel Illumination

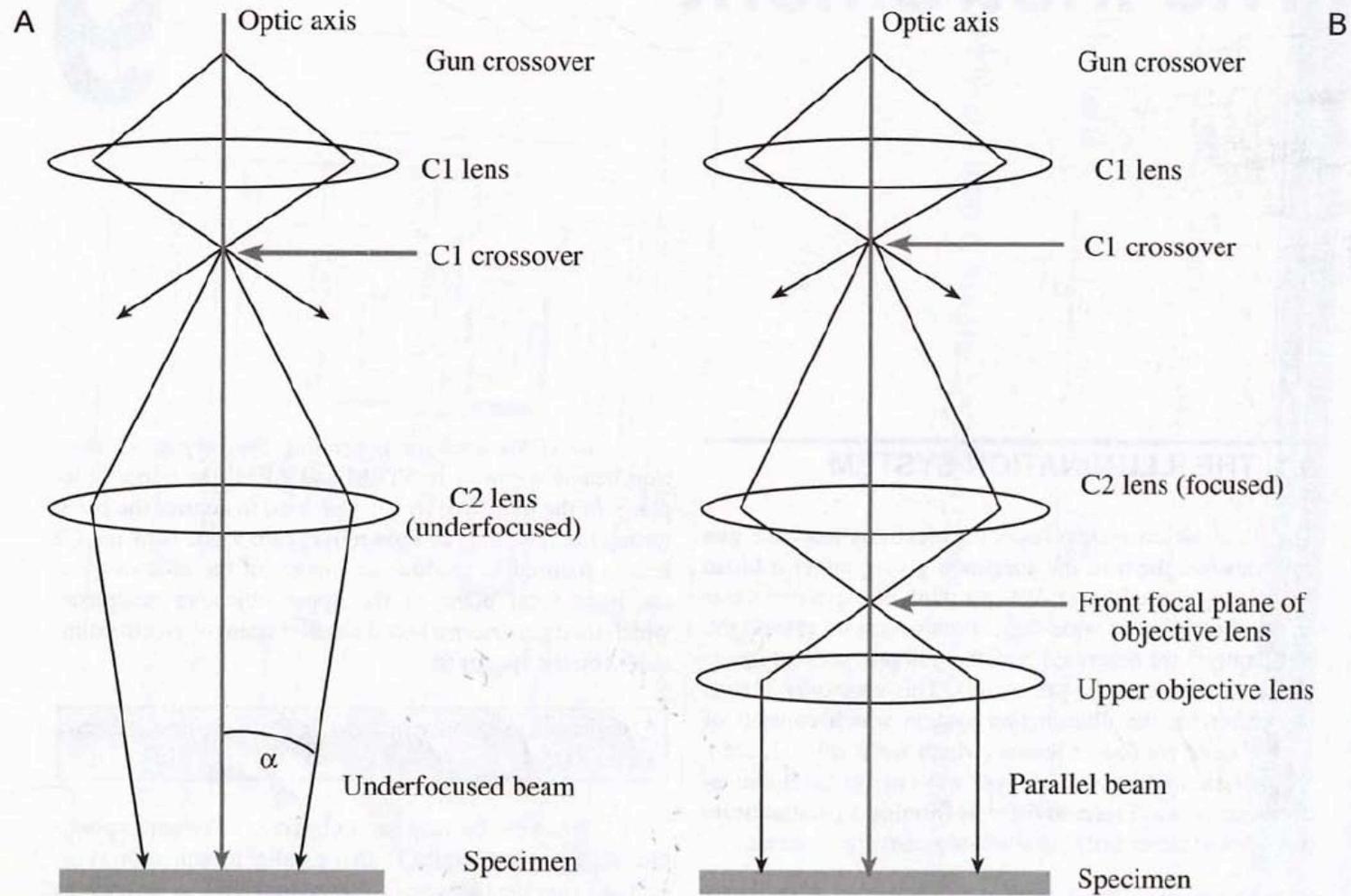


Figure 9.1. Parallel-beam operation in the TEM (A) using just the C1 and an underfocused C2 lens and (B) using the C1 and C2 lenses to image the source at the front focal plane of the upper objective lens.

Place an aperture in the Image Plane this defines an area back projected onto the specimen

Selected-Area Diffraction

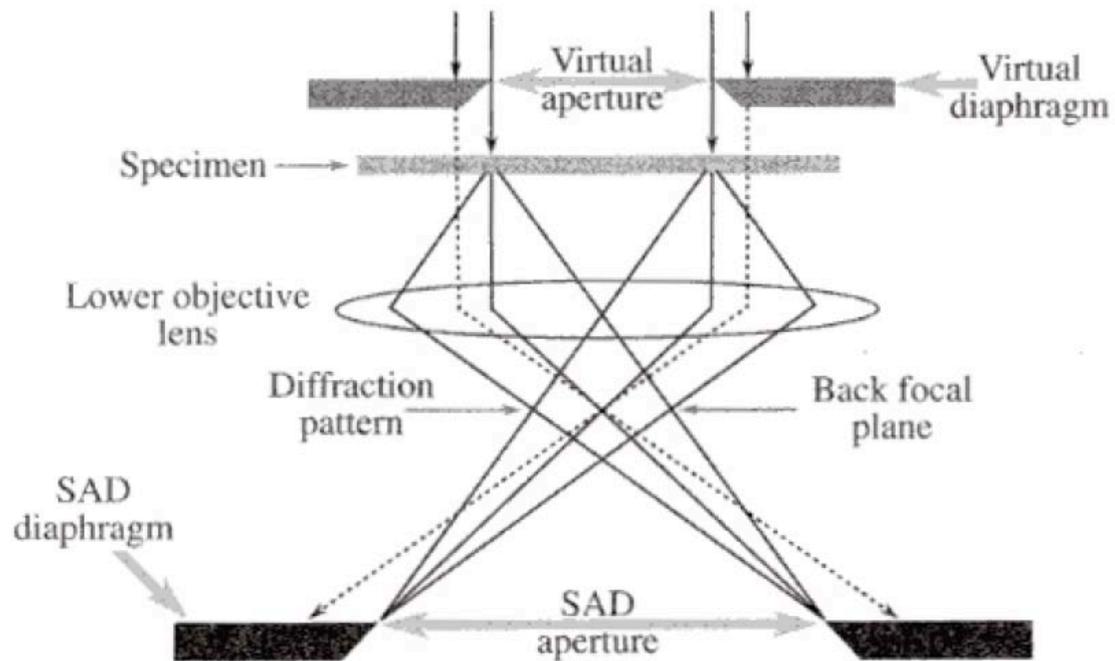
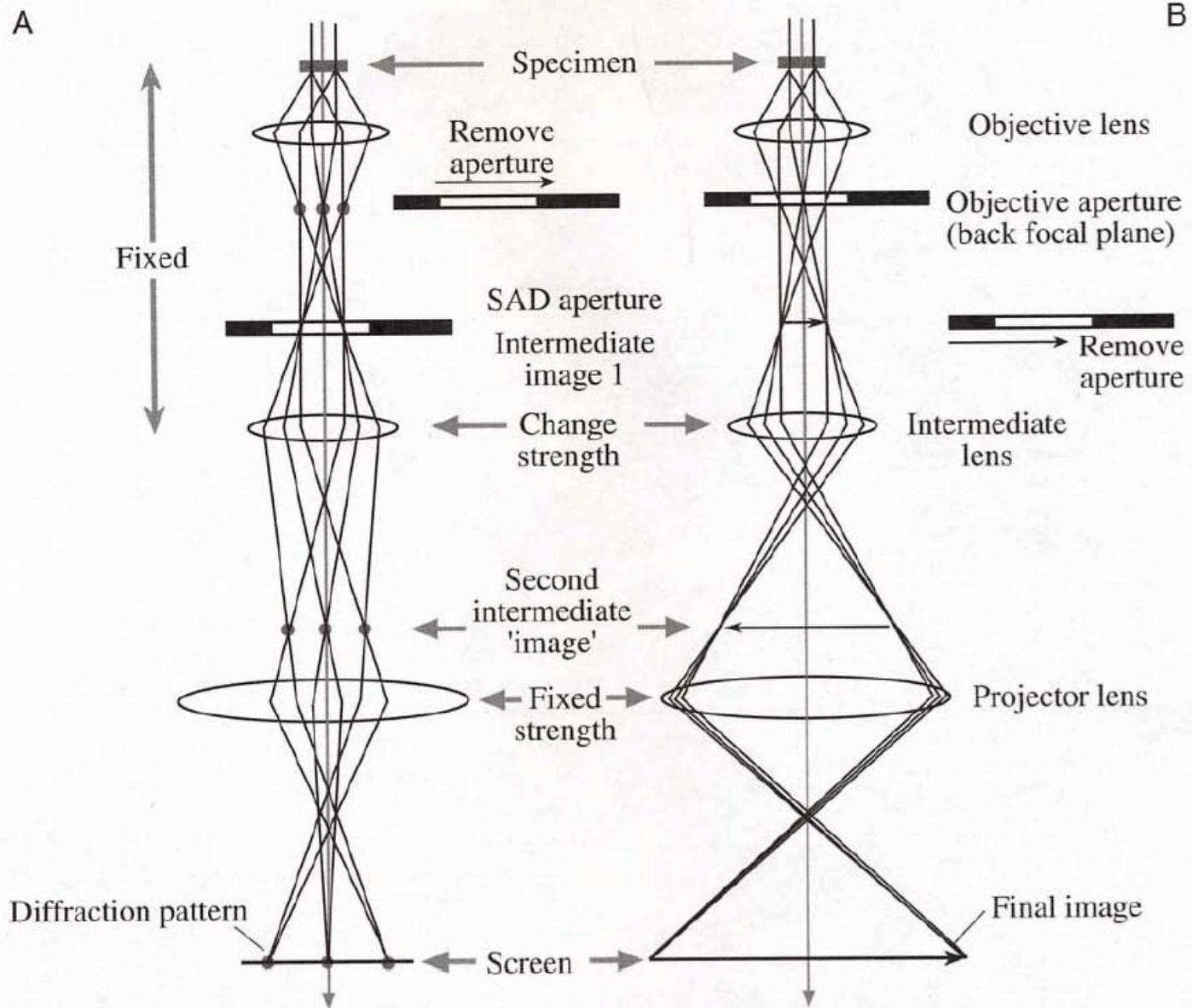


Figure 9.13. Ray diagram showing SAD pattern formation: the insertion of an aperture in the image plane results in the creation of a virtual aperture in the plane of the specimen. Only electrons falling inside the dimensions of the virtual aperture at the specimen will be allowed through into the imaging system. All other electrons will hit the SAD diaphragm.



Why CBED? Why not SAD?

Limits of Conventional SAD

Conventional SAD uses an aperture to define the area from which the pattern is to be recorded. The aperture is placed in the image plane of the objective lens to create a virtual aperture in the specimen plane (Le Poole 1947). The spatial resolution in SAD is limited by both spherical aberration and the ability of the operator to focus the aperture of the and the image in the same plane. The error in area selection U is given by:

$$U = C_s(2\theta_B)^3 + D2\theta_B$$

where: C_s = spherical aberration coefficient

θ_B = Bragg angle

D = minimum focus step.

The result is that the theoretical lower limit of area selection is $\sim 0.5\mu\text{m}$ (in practice governed by aperture size).

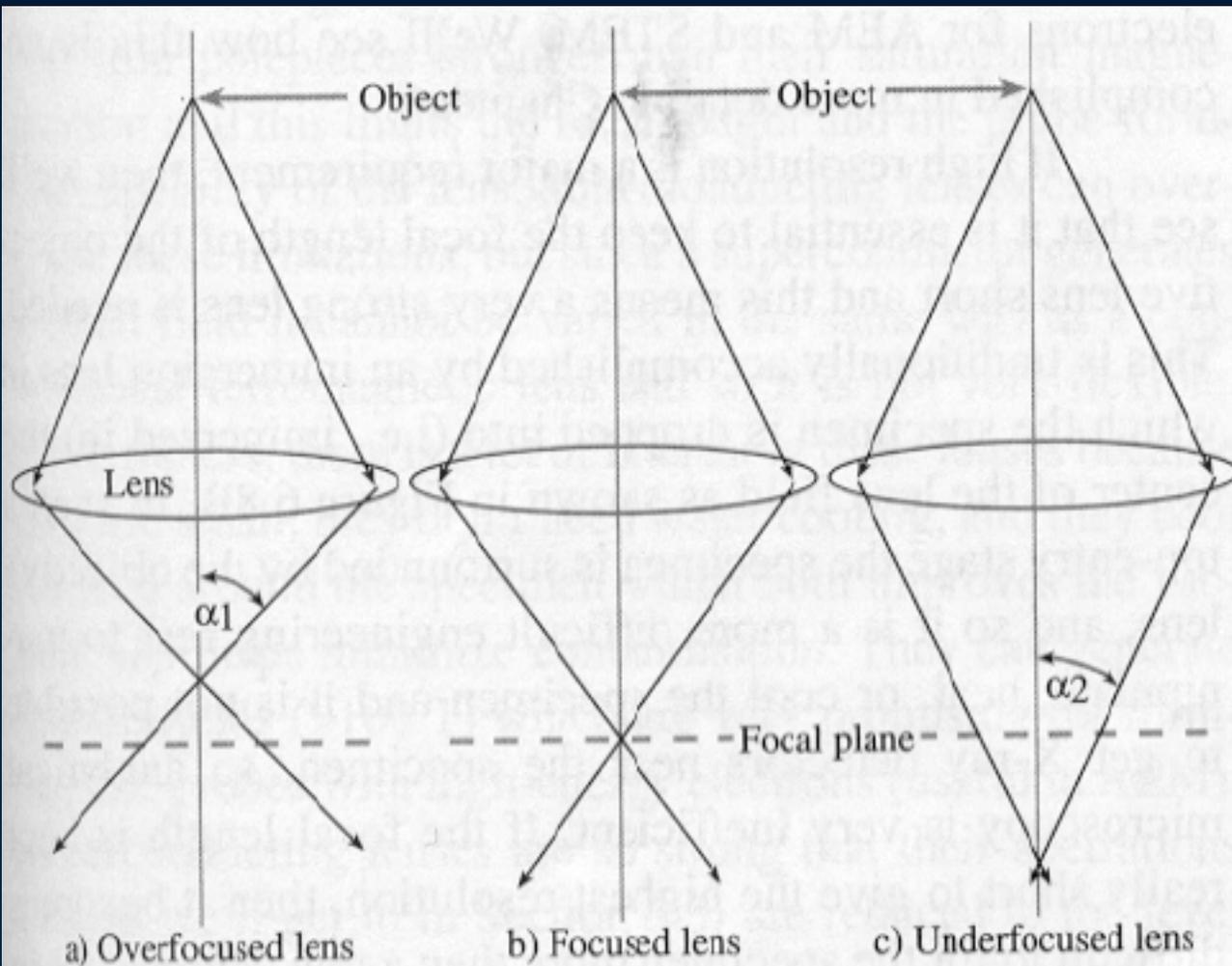
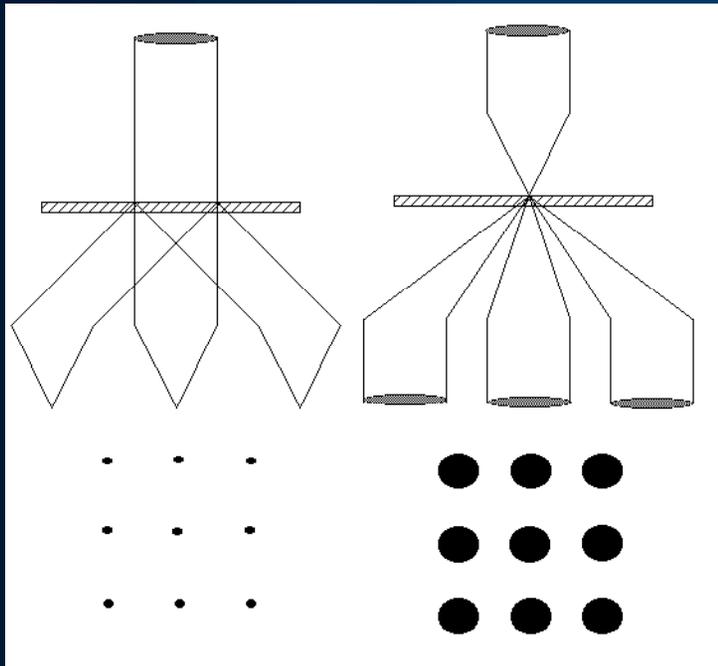
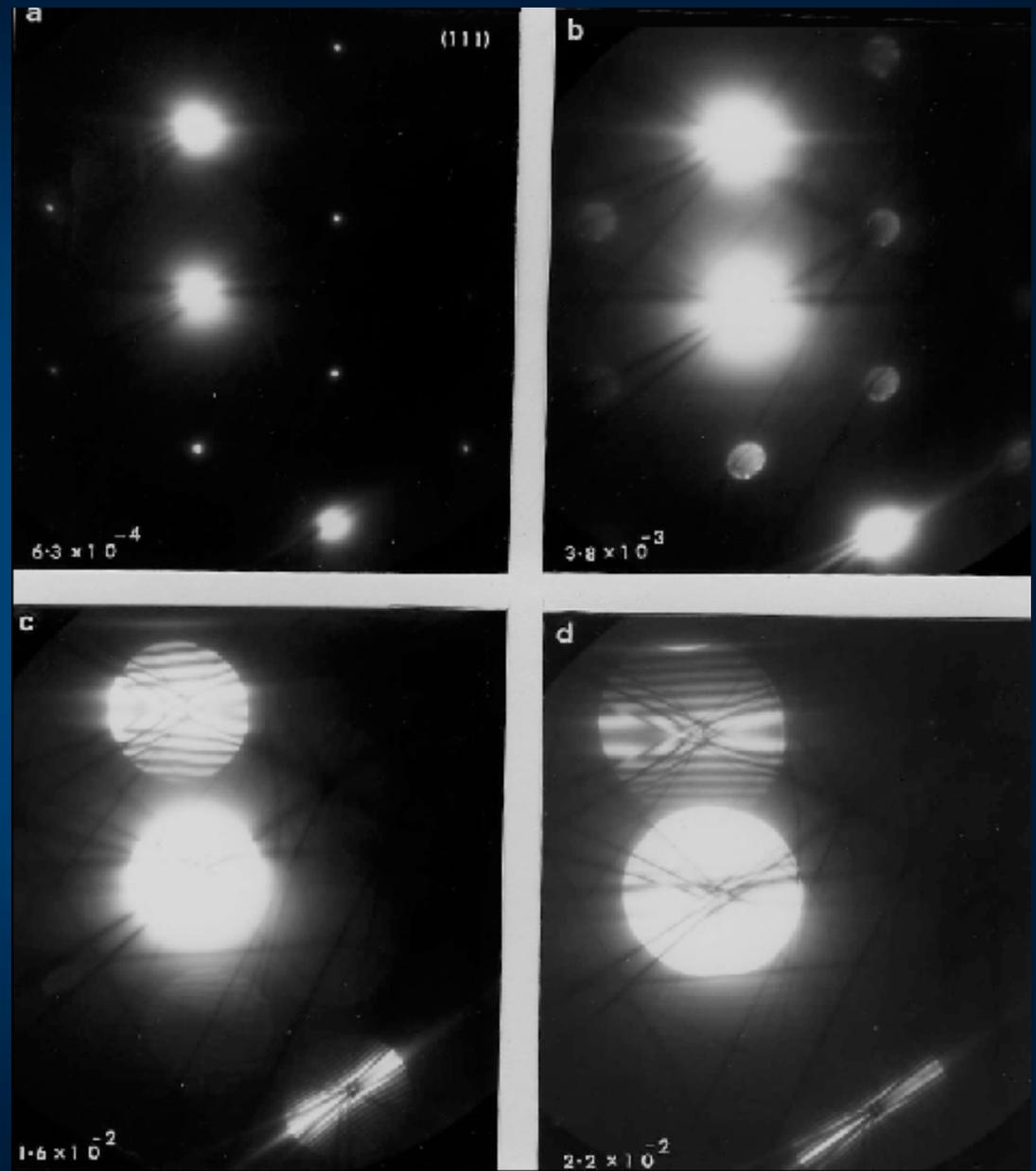
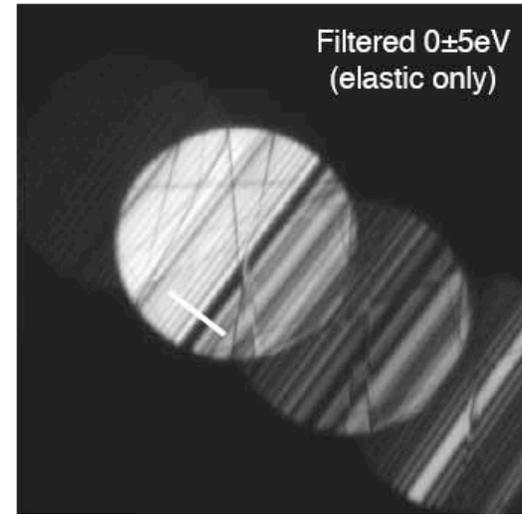
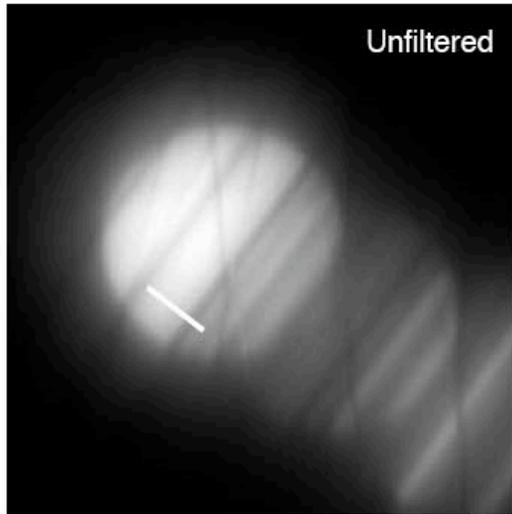


Figure 6.5. (a) Ray diagram illustrating the concepts of overfocus, in which a strong lens focuses the rays before the image plane, and (c) underfocus, where a weaker lens focuses after the image plane. It is clear from (c) that at a given underfocus the convergent rays are more parallel than the equivalent divergent rays at overfocus ($\alpha_2 < \alpha_1$).

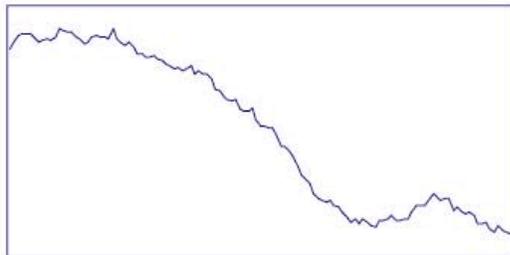


Notice, loss of definition of weak reflections !

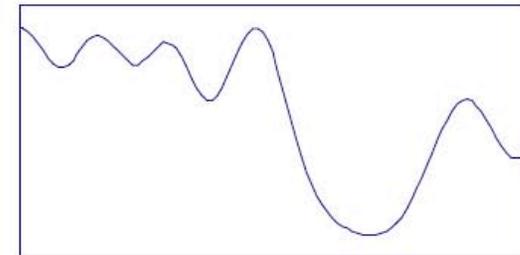




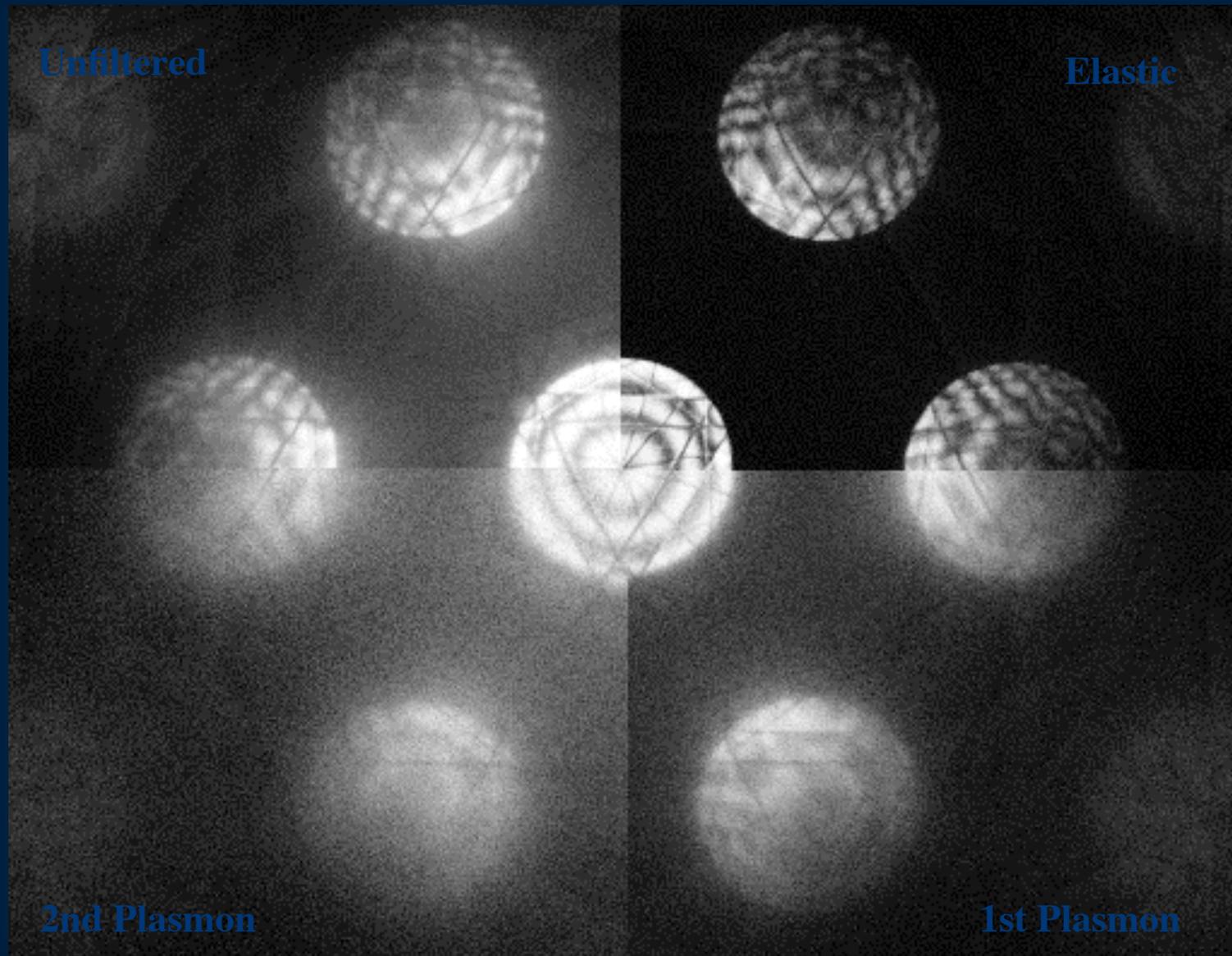
Silicon [110]



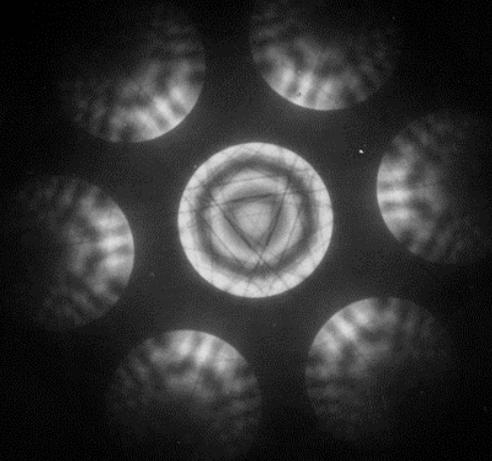
essential for
quantitative CBED



Silicon 111 ZAP- Energy Filtered

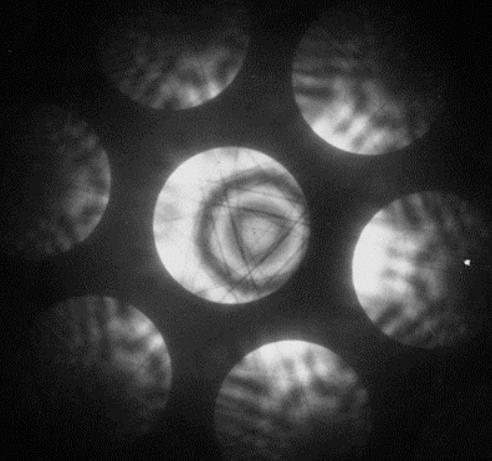


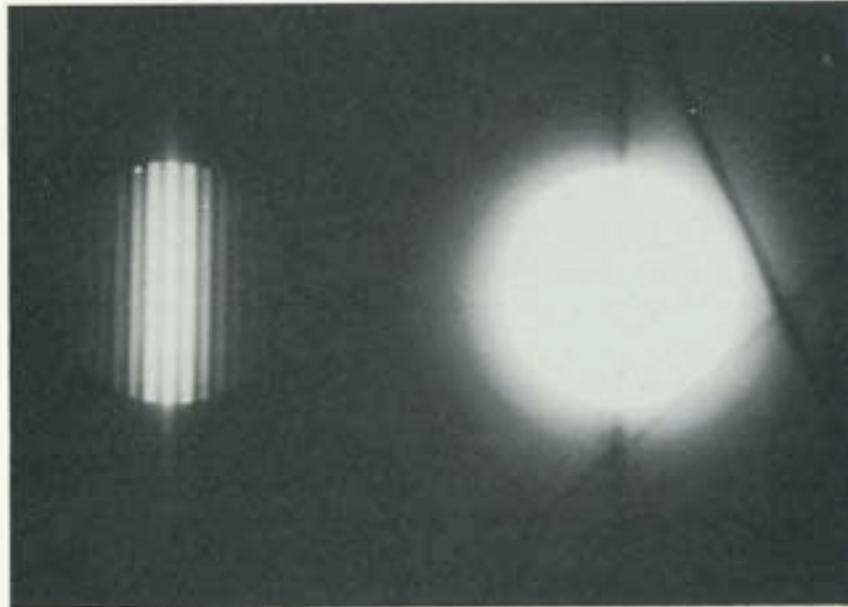
Si [111]



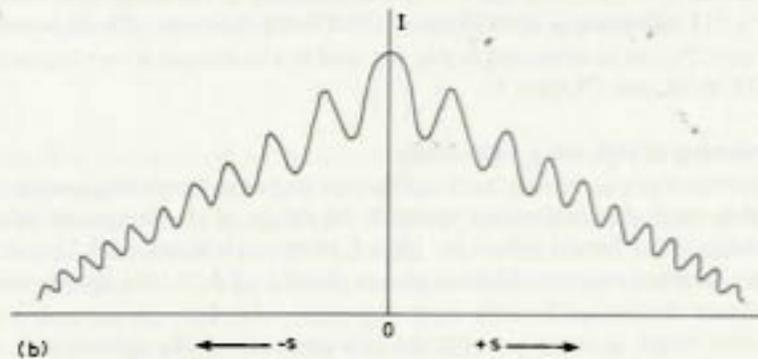
CBED is extremely sensitive to orientation and is the best way to set the exact orientation

Si [111]
Off axis





(a)



(b)

Fig. 4.9 (a) Magnified image of a convergent beam diffraction pattern taken from aluminium at 120 kV. The diffracted beam shows minima corresponding to those in (b). The precise positions of the minima depend on the foil thickness (cf. equation (4.5)).

Theoretical Considerations for Thickness Measurement

Convergent beam diffraction discs are maps of diffracted intensity as a function of incident wave angle and therefore have a direct correspondence to a rocking curve. In the two-beam approximation the rocking curve for the diffracted intensity $|\phi|^2$ is given by (Hirsch et al. 1965):

$$|\phi|^2 = \sin^2 \beta \pi \Delta k z \quad (1)$$

Where:

$$\beta = \tan^{-1} \left(\frac{1}{s \xi_g} \right) \quad \Delta k = \frac{\sqrt{1 + (s \xi_g)^2}}{\xi_g}$$

s is the deviation parameter, ξ_g is the extinction distance and z the foil thickness.

Differentiation with respect to s reveals that the minima of $|\phi|^2$ in equation (1) obey the relationship:

$$\Delta kz = \text{integer} \quad (2a)$$

and the maxima obey the relationship:

$$\tan \pi \Delta kz = \pi \Delta kz \quad (2b)$$

Also, $s=0$ is always either a maximum or minimum. Kelly et al. (1975) expressed equation (2a) as:

$$\left(\frac{s_i}{n_k}\right)^2 = -\left(\frac{1}{\xi}\right)^2 \left(\frac{1}{n_k}\right)^2 + \left(\frac{1}{z}\right)^2 \quad (3a)$$

It is evident that a plot of $\left(\frac{s_i}{n_k}\right)^2$ against

$\left(\frac{1}{n_k}\right)^2$ in a two-beam condition yields a

straight line with intercept $\left(\frac{1}{z}\right)^2$ and slope

of $\left(\frac{1}{\xi}\right)^2$. This is the basis of the CBED

thickness measurement technique that is now well known.

P.M. Kelly et al.,
Phys. Stat. Sol.
(1975)A31, 771.

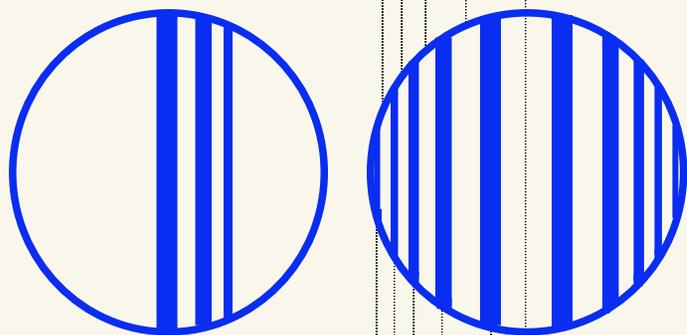


Si $\langle 220 \rangle$ @ 200 kV
 $a=0.543$ nm
 $t \sim 280$ nm $\xi \sim 125$ nm

$$\left(\frac{S_i}{X_{k'}}\right)^2 = -\left(\frac{1}{\xi}\right)^2 \left(\frac{1}{X_{k'}}\right)^2 + \left(\frac{1}{Z}\right)^2$$

Equation for sequence of maxima where:

$$s_i = \frac{\lambda \Delta\theta}{d^2 2\theta_d}$$



$$\left(\frac{S_i}{n_k}\right)^2 = -\left(\frac{1}{\xi}\right)^2 \left(\frac{1}{n_k}\right)^2 + \left(\frac{1}{Z}\right)^2$$

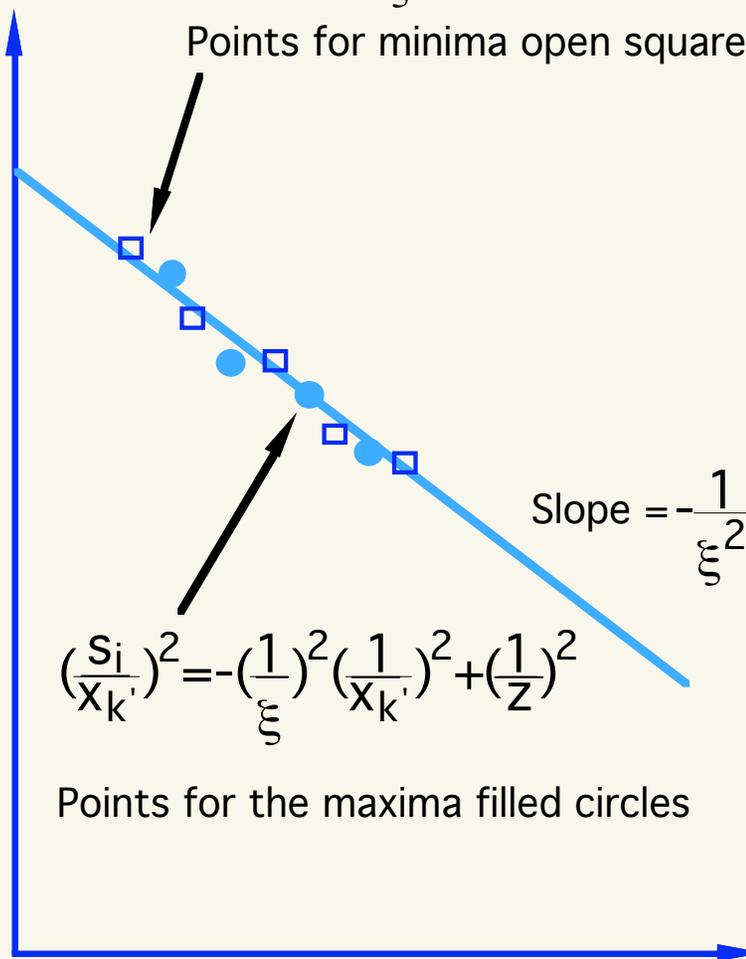
Equation for sequence of minima where:

$$s_i = \frac{\lambda \Delta\theta}{d^2 2\theta_d}$$

$$\left(\frac{S_i}{n_k}\right)^2 = -\left(\frac{1}{\xi}\right)^2 \left(\frac{1}{n_k}\right)^2 + \left(\frac{1}{Z}\right)^2$$

Points for minima open squares

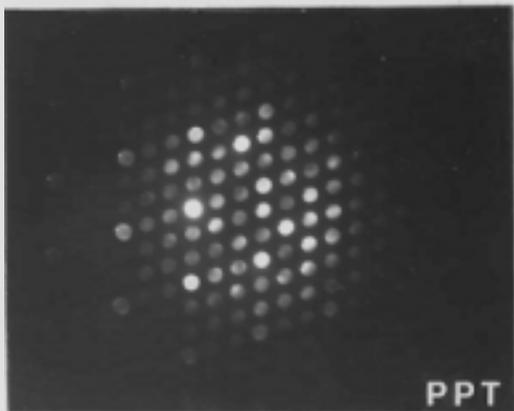
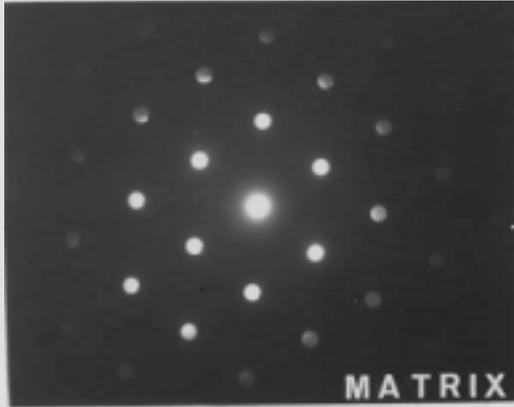
Intercept
 $\frac{1}{Z^2}$



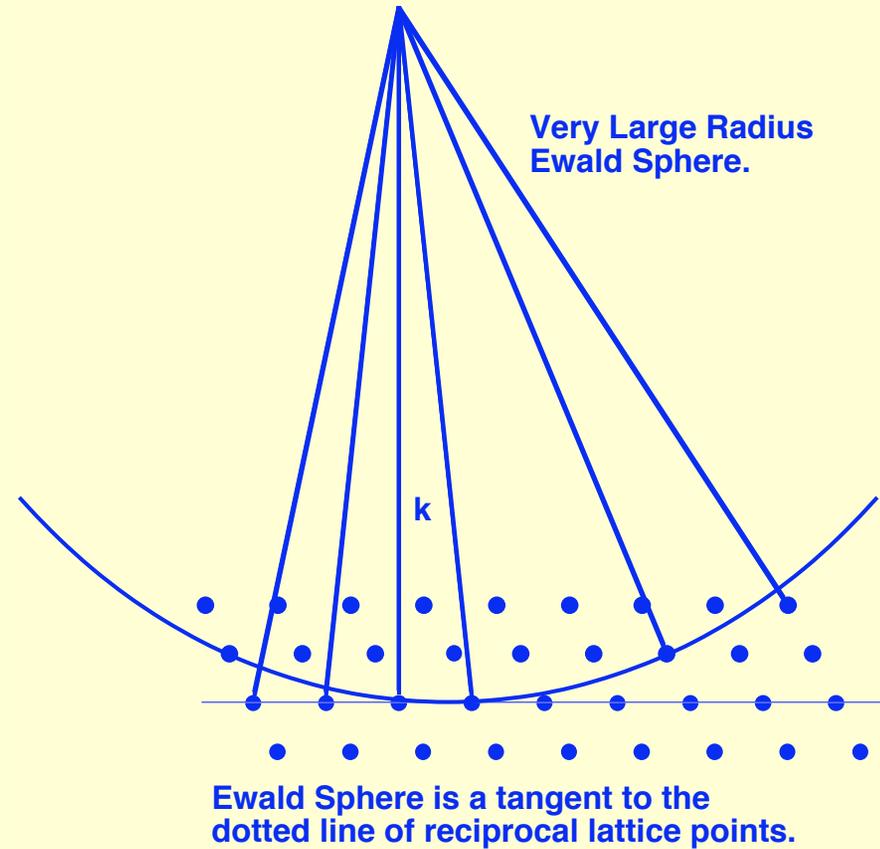
$$\left(\frac{S_i}{X_{k'}}\right)^2 = -\left(\frac{1}{\xi}\right)^2 \left(\frac{1}{X_{k'}}\right)^2 + \left(\frac{1}{Z}\right)^2$$

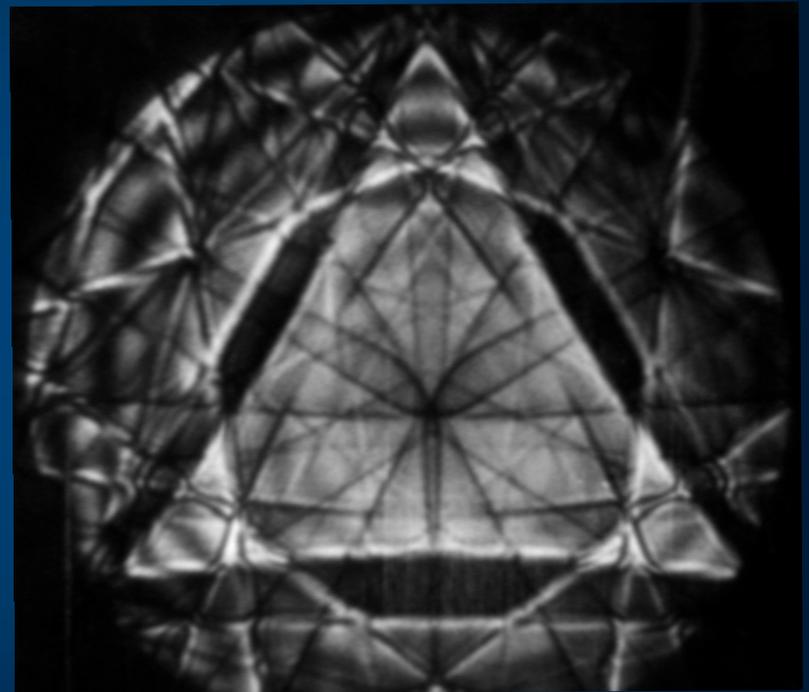
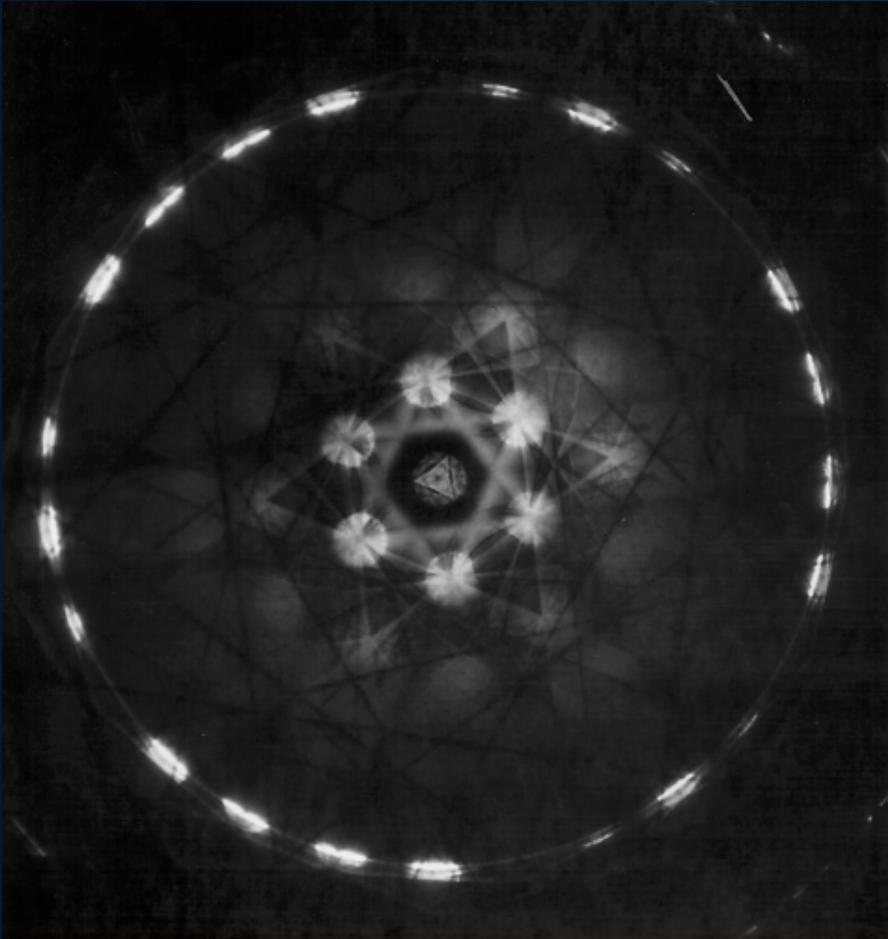
Points for the maxima filled circles

Diffracted Intensity Falls off with angle because of Ewald Sphere



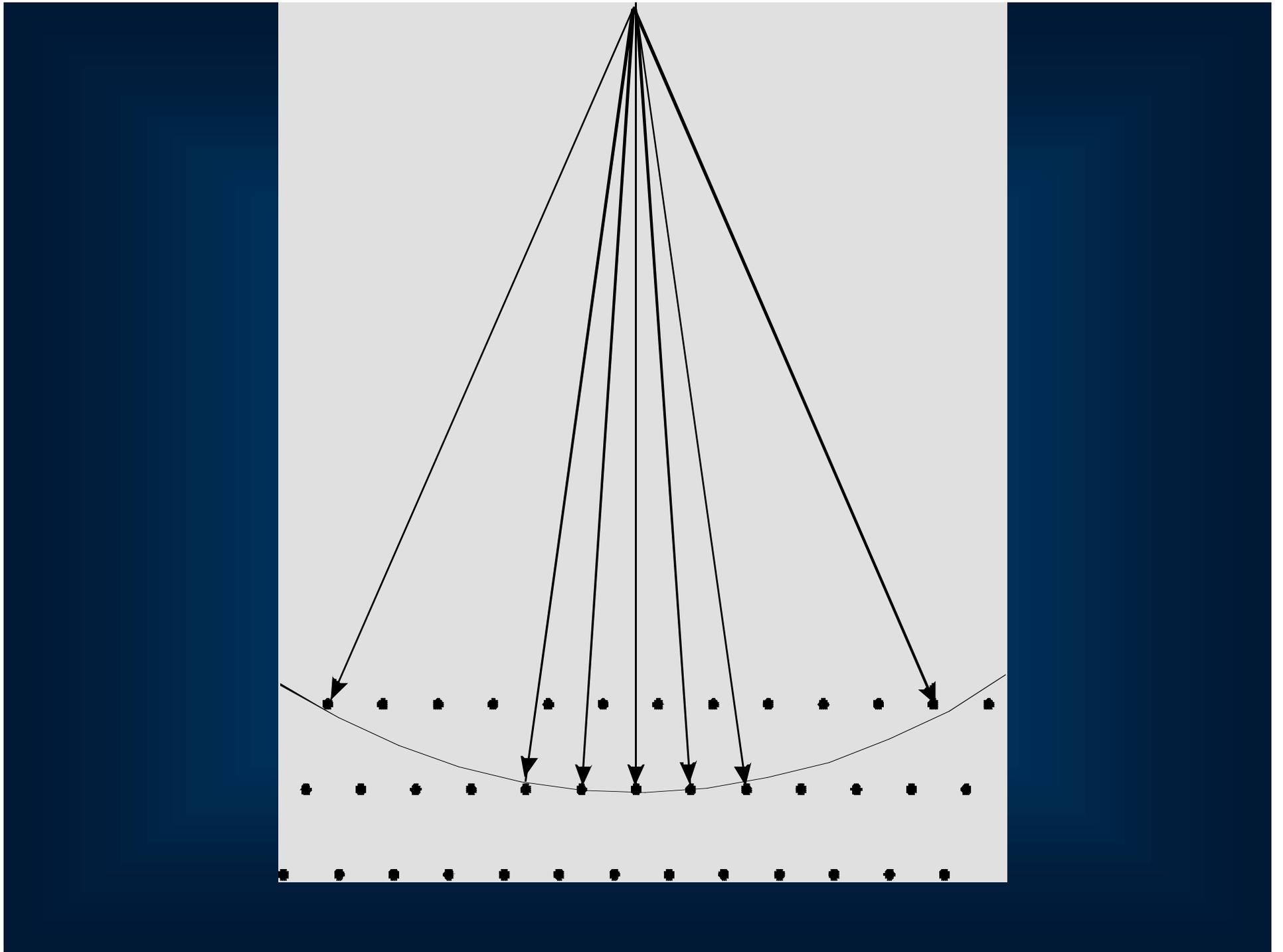
High Energy Electron Case.





Laue Zones

- At a zone-axis orientation, the reflections in the diffraction pattern break up into zones called Laue zones
- The central zone is called the zero-order Laue zone
- The first ring is called the first-order Laue zone - and so on
- The first-order, second-order, third order (and so on) are known collectively as the higher-order Laue zones

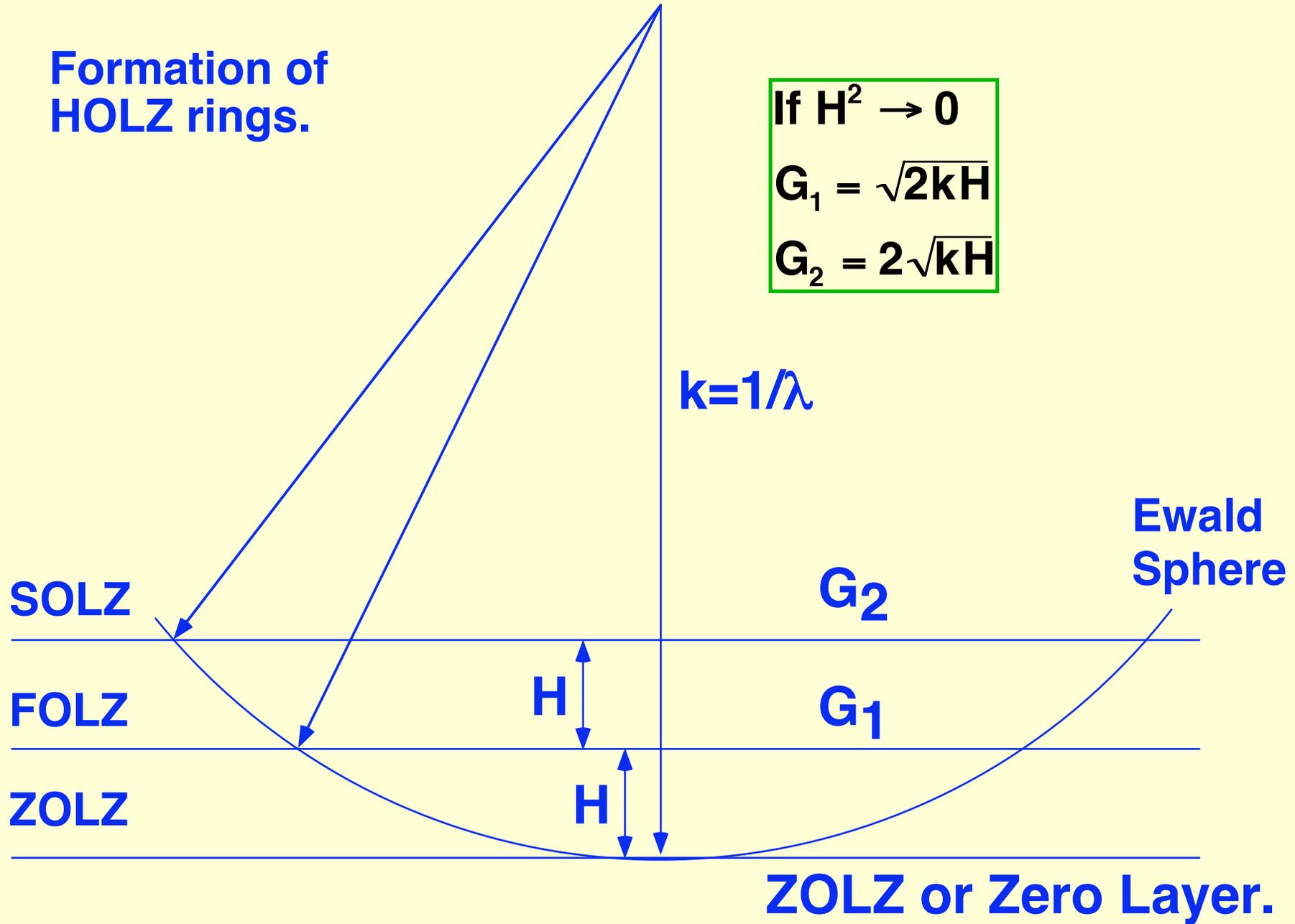


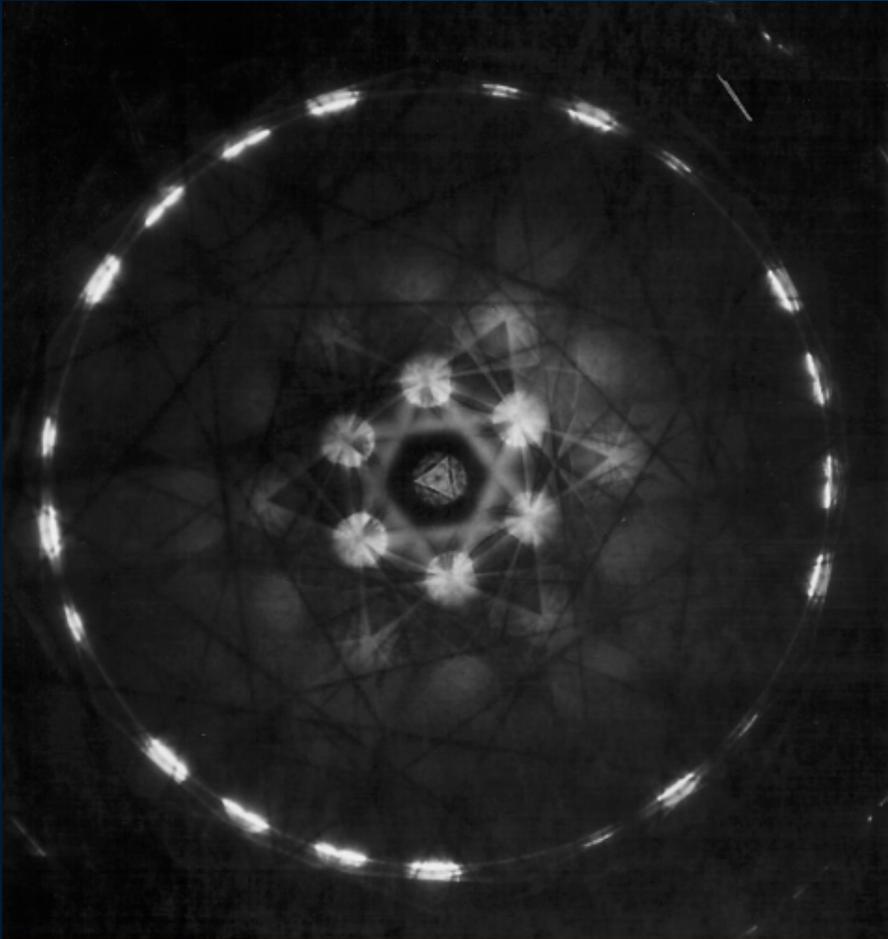
HOLZ

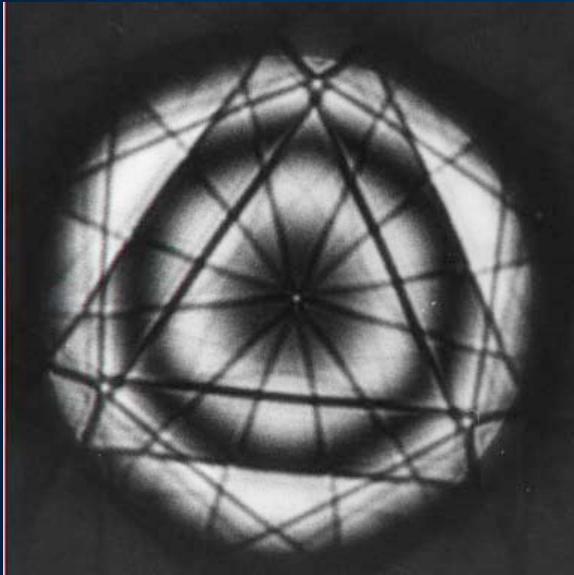
- HOLZ is the acronym for higher-order Laue zone
- The rings of reflections outside the central, zero-order Laue zone are the HOLZ
- Because the narrow, dark, straight lines in the bright field disc are associated with diffraction into a HOLZ reflection, they are known as HOLZ lines
- Do not confuse HOLZ with HOLZ lines

Formation of HOLZ rings.

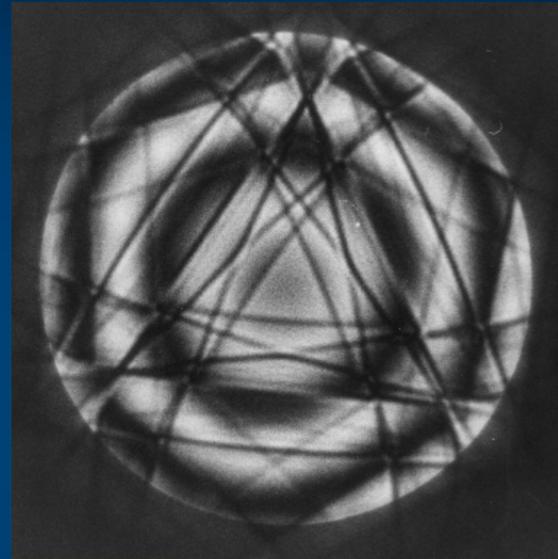
$$\text{If } H^2 \rightarrow 0$$
$$G_1 = \sqrt{2kH}$$
$$G_2 = 2\sqrt{kH}$$





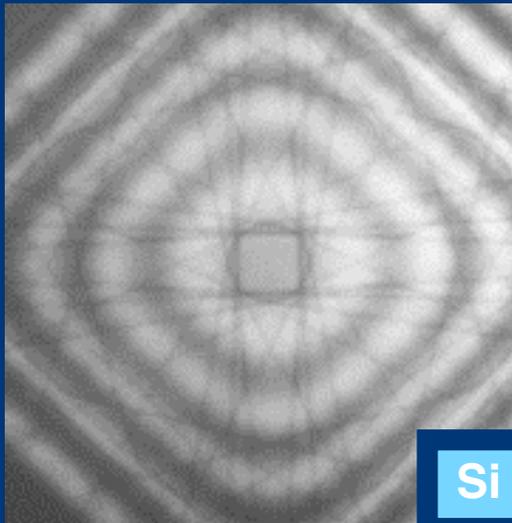


113 kV

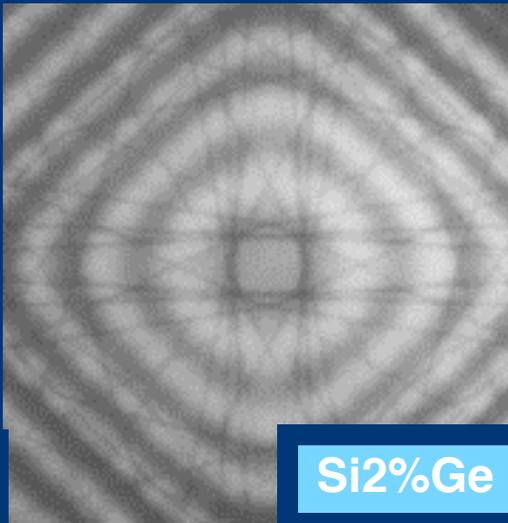


100 kV

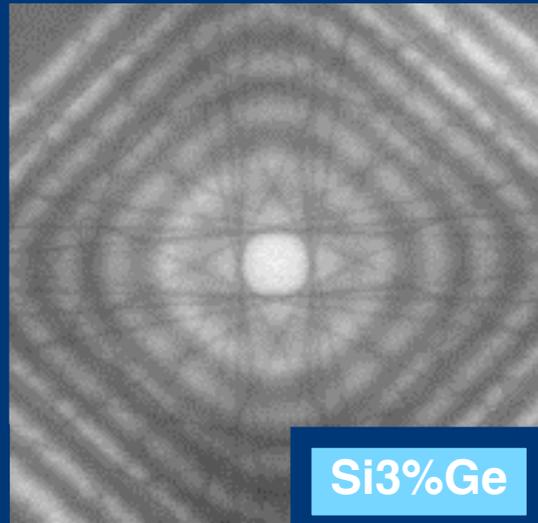
$\langle 001 \rangle$ CBED ZAPs from Si & SiGe Alloys



Si

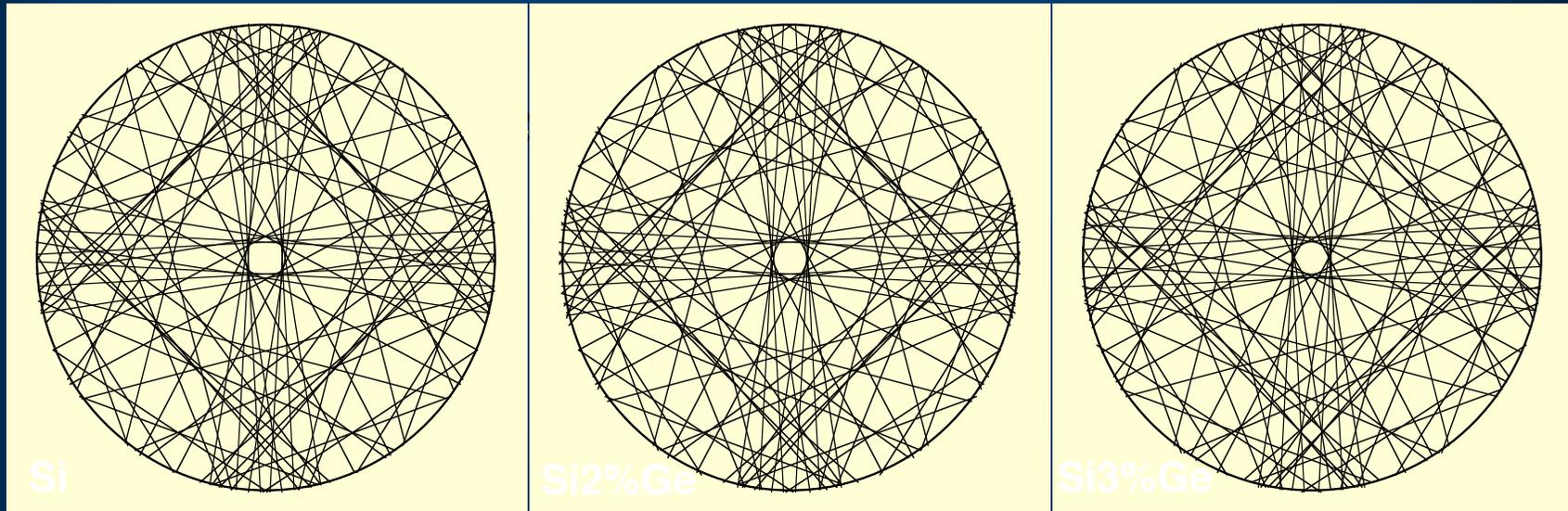


Si2%Ge



Si3%Ge

CBED ZAPs from Si, Si2%Ge & Si3%Ge cross section samples. Center of direct disc. Patterns recorded at 150kV, with a beam convergence of ~ 8 mrad. Probe diameter ~ 30 nm. Samples were held at liquid nitrogen temperature to reduce the thermal diffuse scattering. The orthorhombic distortion of the lattice is most obvious in the Si2%Ge sample.



CBED Simulations based on the kinematical approximation for Si, Si2%Ge and Si3%Ge. $\langle 001 \rangle$ zone axis pattern, convergence angle approximately 10mrad. Voltage set to 149.5kV by comparison with the Si pattern.

Lattice parameters:

Silicon $a=0.5429\text{nm}$, Si2%Ge $a=0.5434\text{nm}$ $b= 0.5429\text{nm}$ $c= 0.5430\text{nm}$

Si3%Ge $a= 0.5445\text{nm}$ $b= 0.5440\text{nm}$ $c= 0.5440\text{nm}$

HOLZ Plots
generated by Diffract™